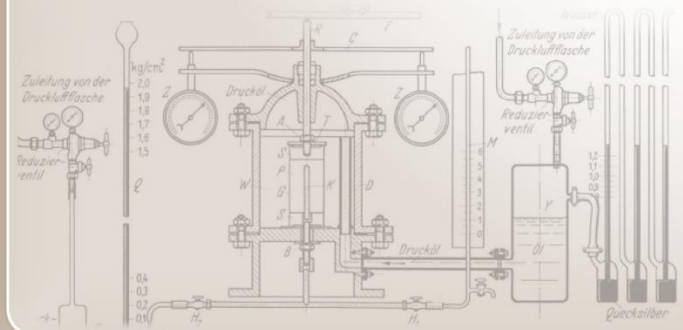
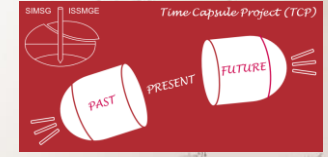
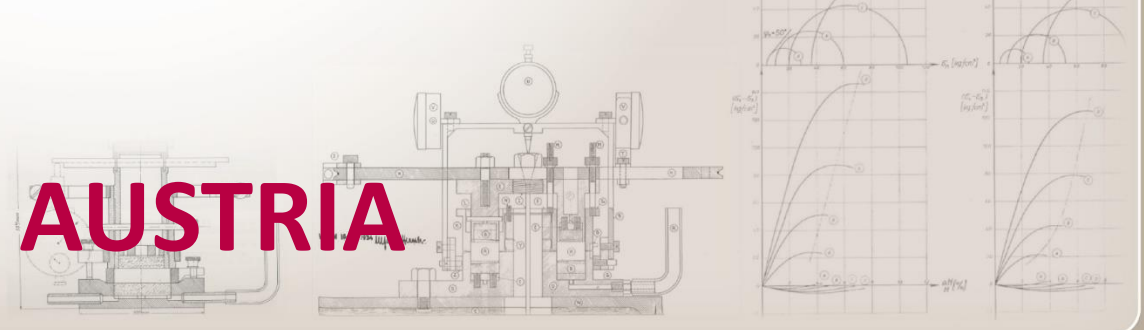


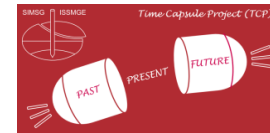
VIENNA

Time Capsule Project (TCP)



AUSTRIA





Introduction

This series of slides presents a selection of important achievements and activities of the Austrian Geotechnical Society as part of the *Time Capsule Project* launched by the ISSMGE.

The **past** is covered by featuring the early days of soil mechanics in the 1920s when Karl von Terzaghi was Professor in Vienna where he established a soil mechanics laboratory together with his co-workers. Some decades later the Institute of Soil Mechanics, Rock Mechanics and Foundation Engineering was established at Graz University of Technology under the leadership of Professor Christian Veder.

Moving towards the **present** Professor Heinz Brandl has to be mentioned who pioneered the integration of Eastern European Countries into the ISSMGE when the iron curtain was still a barrier for free travel.

Looking into the **future** ongoing research activities of key university institutes of geotechnics are highlighted showing a variety of topics covering many aspects of soil mechanics, geotechnical engineering and computational geotechnics.

A list of selected international projects where specialist contractors based in Austria are involved demonstrates that Austrian technology is applied world wide.

Finally the Austrian section of the Young Member Presidential Group present their way into the **future**.

The contribution towards this presentation of many colleagues, active in the Austrian Geotechnical Society, is gratefully acknowledged.

Helmut F. Schweiger
President Austrian Geotechnical Society

Content

■ Personalities

- Karl von Terzaghi
- Christian Veder
- Heinz Brandl

■ Past and Current Research Activities

- TU Wien (TUW)
- Graz University of Technology (TUG)
- University of Innsbruck (UIBK)
- University of Natural Resources and Life Sciences, Vienna (BOKU)

■ Miscellaneous

- International Projects of Specialist Contractors
- Young Member Presidential Group
- Conferences
- Bid for 21st ICSMGE 2026 in Vienna

PAST

FUTURE

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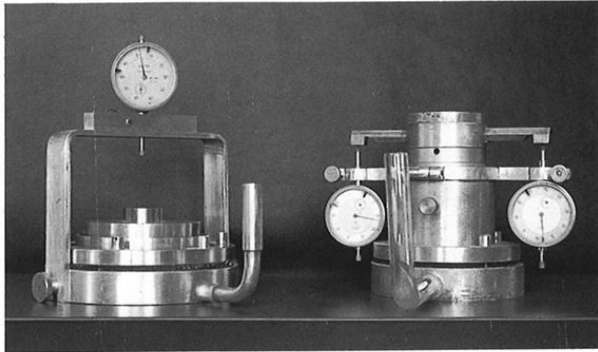
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PAST

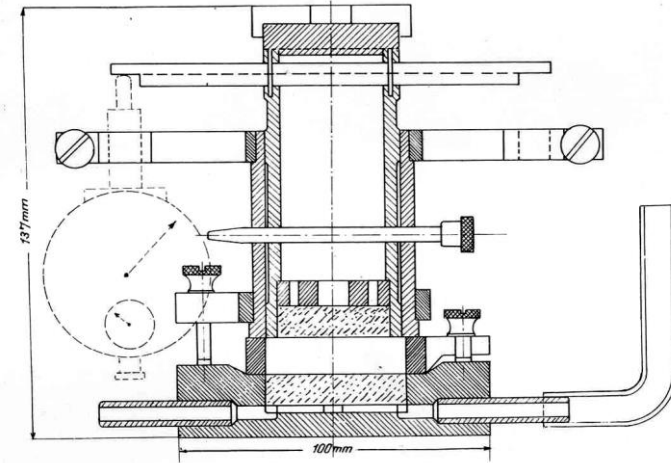
FUTURE

Personalities: Karl von Terzaghi Professor at Vienna Technical University 1929-1938

Arthur Casagrande: Head of Soil Mechanics Laboratory 1929-1932



Original of first oedometer



Original drawing of oedometer

Source:

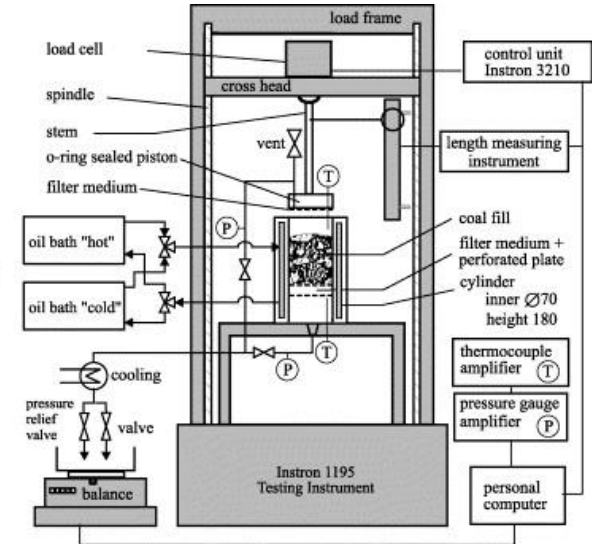
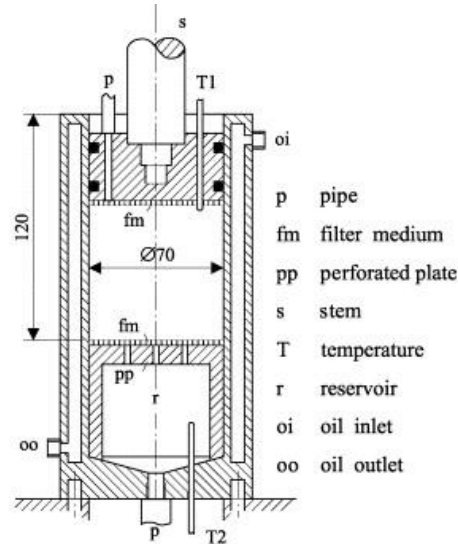
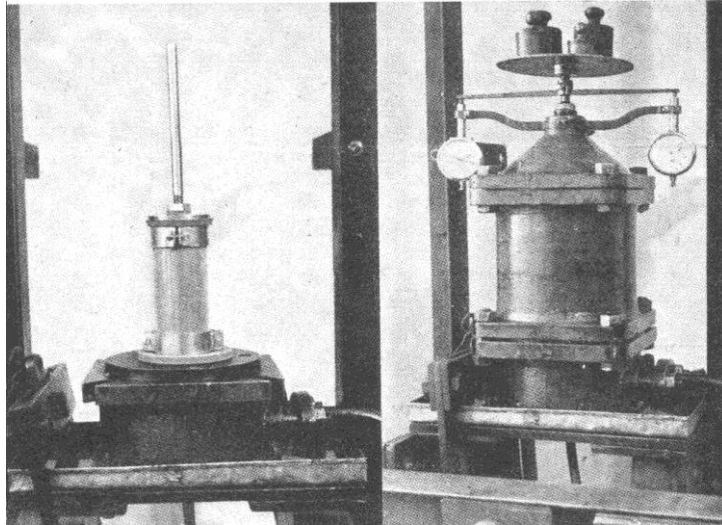
H. Brandl - Prof.Dr.Dr.h.c.mult. Karl v. Terzaghi

H. Brandl - History of the Institute for Foundation Engineering and Soil Mechanics at the Vienna Technical University

Technische Universität Wien - Mitteilungen für Grundbau, Bodenmechanik und Felsbau (1983-1984)

Personalities: Karl von Terzaghi Professor at Vienna Technical University 1929-1938

Arthur Casagrande: Head of Soil Mechanics Laboratory 1929-1932

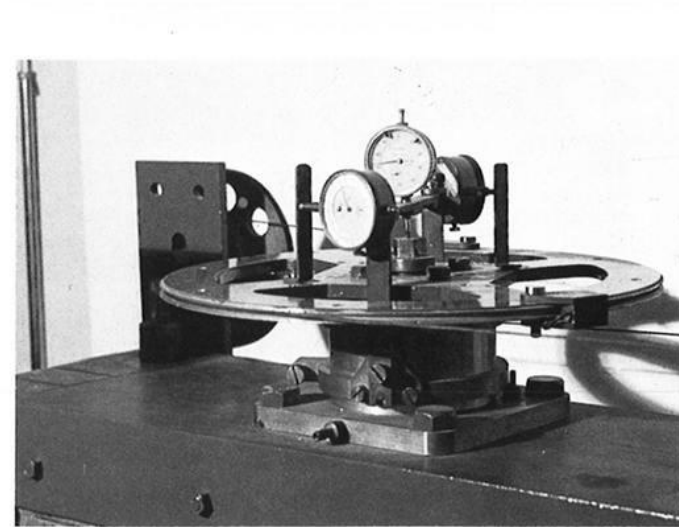


First triaxial compression apparatus, 1934

Personalities: Karl von Terzaghi Professor at Vienna Technical University 1929-1938

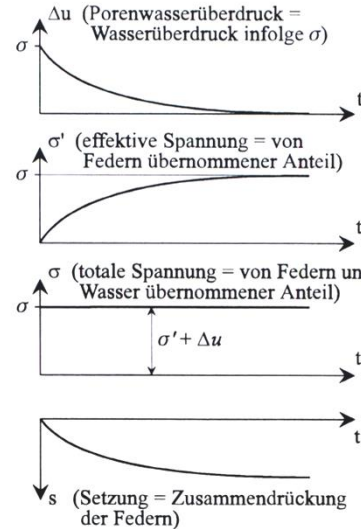
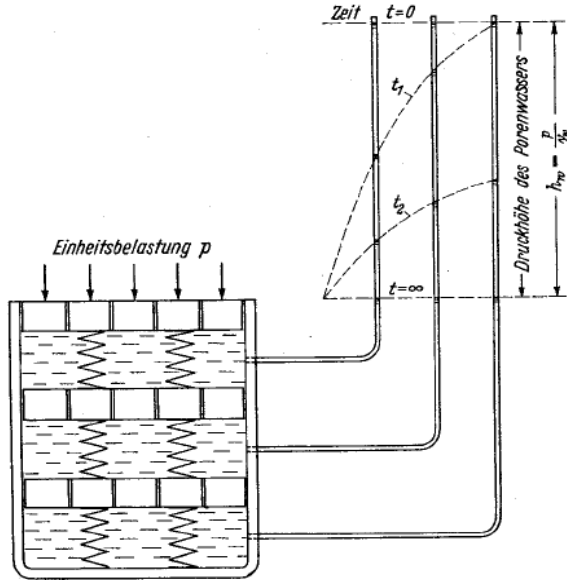


Terzaghi's Laboratory



First ring shear apparatus, 1934

Personalities: Karl von Terzaghi Professor at Vienna Technical University 1929-1938



$$\frac{\partial}{\partial t} \left(\frac{\Delta l}{l} \right) = v \frac{\partial p}{\partial t} = \frac{k}{\gamma} \frac{\partial^2 w}{\partial z^2}$$

$$\frac{\partial p}{\partial t} + \frac{\partial w}{\partial t} = 0 \quad .^8$$

$$\frac{\partial w}{\partial t} = \frac{k}{v\gamma} \frac{\partial^2 w}{\partial z^2} = c \frac{\partial^2 w}{\partial z^2} \quad .^{10}$$

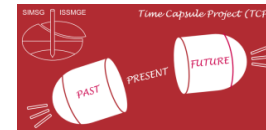
Terzaghi's one-dimensional consolidation theory, 1936



Austrian
Geotechnical
Society

OIAV
AUSTRIAN ASSOCIATION OF
ENGINEERS AND ARCHITECTS

Time Capsule Project (TCP)

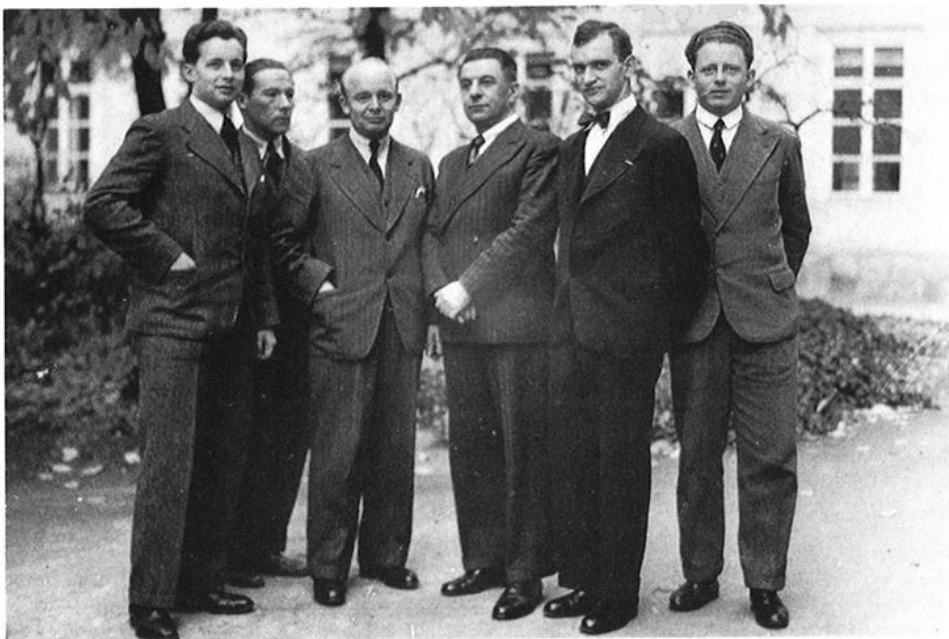


10

Personalities: Karl von Terzaghi Professor at Vienna Technical University 1929-1938

Otto K. Fröhlich: Professor at Vienna Technical University 1940-1956

Hubert Borowicka: Professor at Vienna Technical University 1957-1980



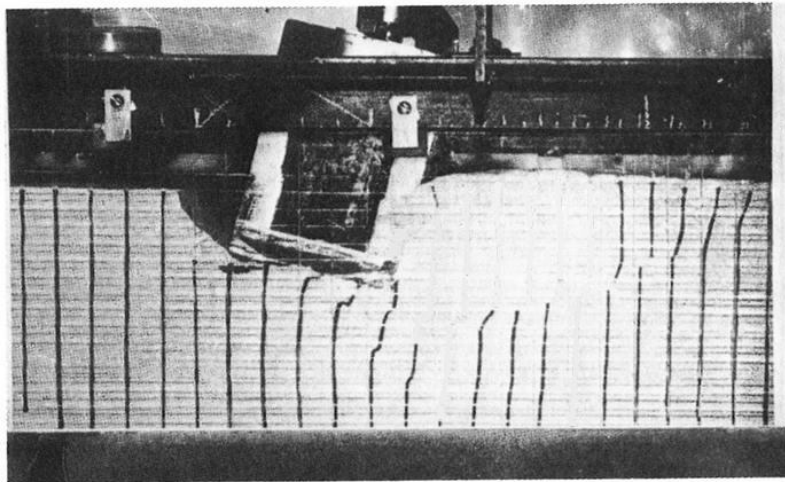
Co-workers of K.v.Terzaghi in Vienna, 1935

K. Kienzl, O. Schwarz, J. Hvorslev, O.K. Fröhlich,
H. Borowicka, W. Steinbrenner

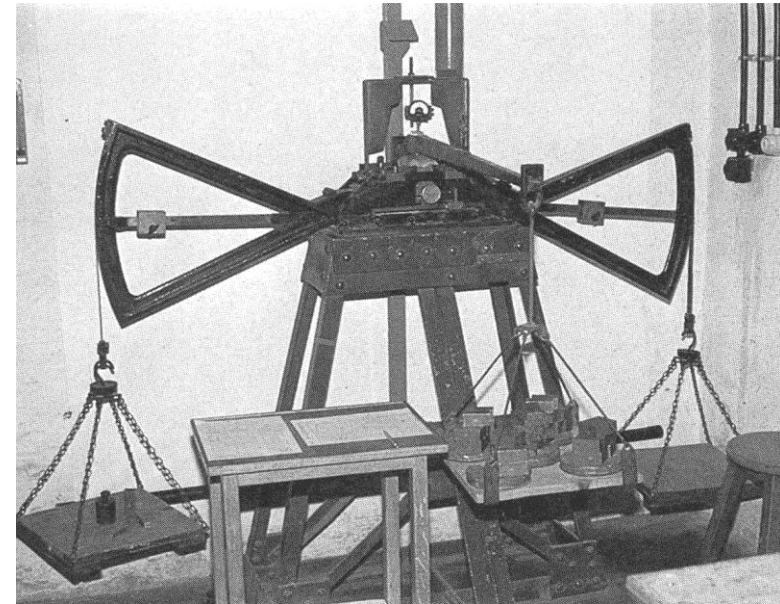
Personalities: Karl von Terzaghi Professor at Vienna Technical University 1929-1938

Otto K. Fröhlich: Professor at Vienna Technical University 1940-1956

Hubert Borowicka: Professor at Vienna Technical University 1957-1980



Laboratory experiment of bearing capacity of footings under inclined loading
A.R. Jumikis and O.K. Fröhlich



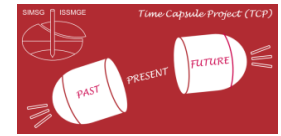
Shear box test apparatus
“Vienna routine shear test”
(After Hubert Borowicka)



Austrian
Geotechnical
Society

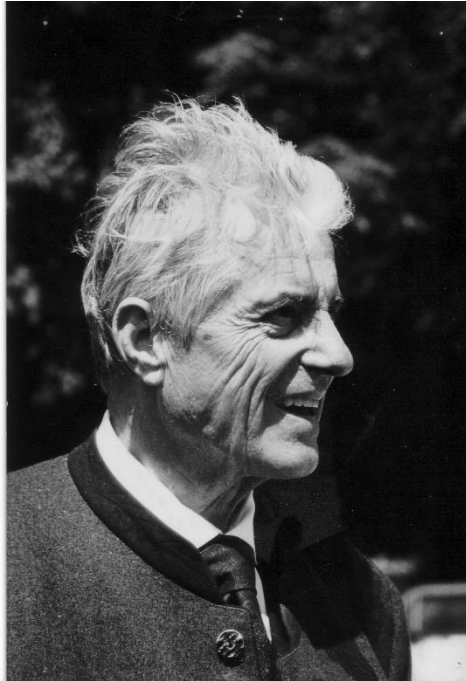
OIAV
AUSTRIAN ASSOCIATION OF
ENGINEERS AND ARCHITECTS

Time Capsule Project (TCP)



12

Personalities: Christian Veder Professor at Graz University of Technology 1964-1978

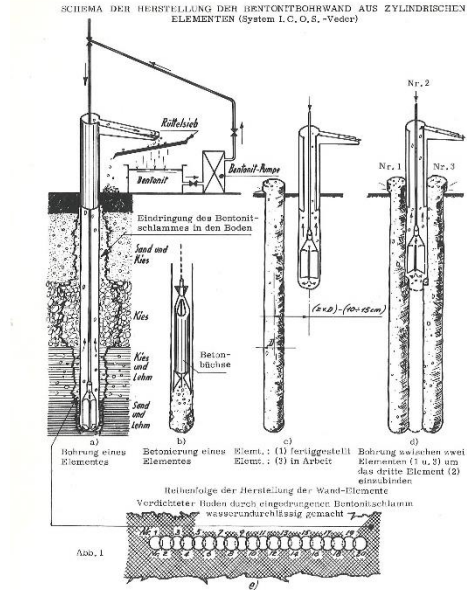


Christian Veder 1907-1984

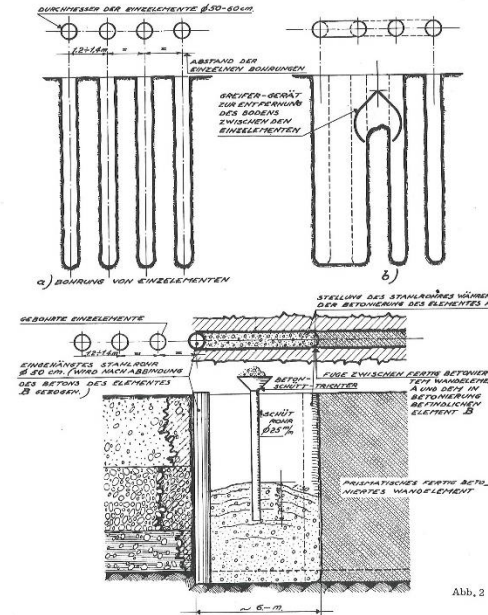


Christian Veder and Karl v. Terzaghi

Inventor of diaphragm wall technique



SCHEMA DER HERSTELLUNG DER BENTONITBOHRWAND AUS PRISMATISCHEN ELEMENTEN (System I.C.O.S., -Veder)



Source:

Ch. Veder: *Neue Verfahren zur Herstellung von untertägigen Wänden und Injektionsschirmen in Lockergesteinen und durchlässigem Fels*
Mitteilungen des Institutes für Wasserwirtschaft, Grundbau und Konstruktiven Wasserbau der Technischen Hochschule Graz, 1959

Inventor of diaphragm wall technique

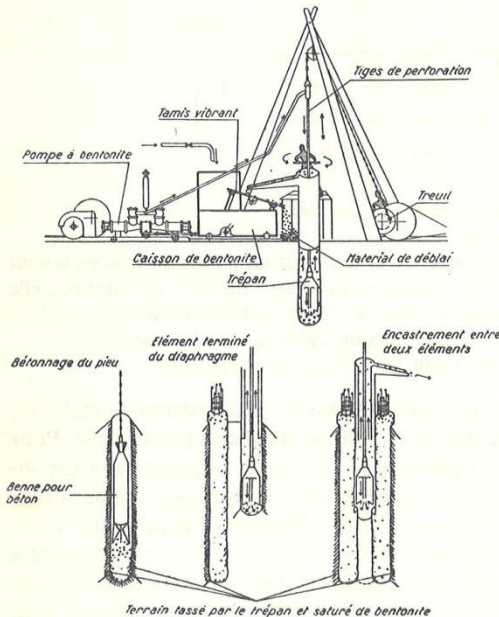


Fig. 1 Schéma d'exécution du diaphragme imperméable
Construction of the Impervious Diaphragm

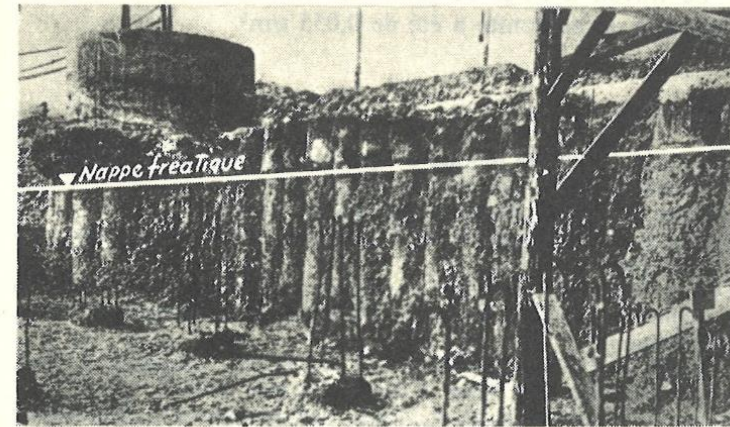


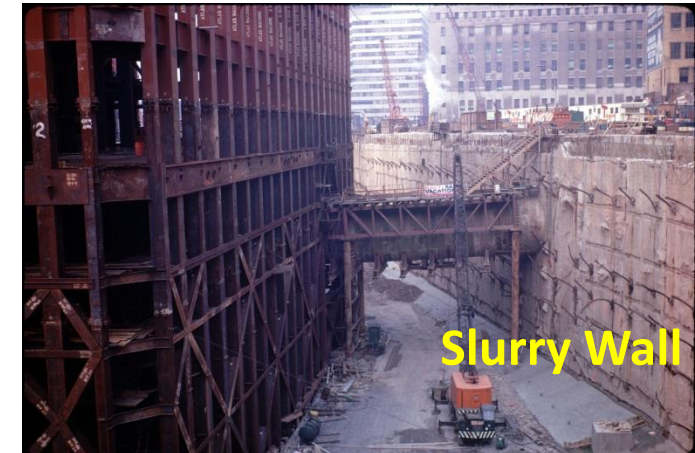
Fig. 3 Vue du diaphragme en béton partiellement découvert – Chantier de Volturmo
Concrete Diaphragm Partly Uncovered on the Volturmo Building Site

Specialist contractor I.C.O.S., Milano, Italy: first applications of diaphragm walls in late 1940s

Ch. Veder: *Neue Verfahren zur Herstellung von untertägigen Wänden und Injektionsschirmen in Lockergesteinen und durchlässigem Fels*
Mitteilungen des Institutes für Wasserwirtschaft, Grundbau und
Konstruktiven Wasserbau der Technischen Hochschule Graz, 1959



- 1,000 m long, 900 mm thick
- 158 panels, each ~ 6.7 m wide
- installed in 12 months (1967/68)



Suggestion for stabilising Leaning Tower of Pisa

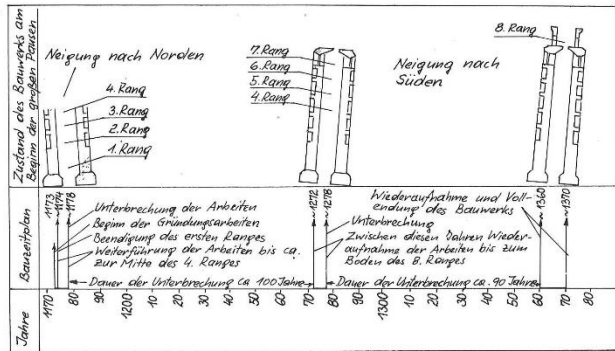


Abb. 1 Bauphasen des Turmes von Pisa (Ricerche e studi, 1971)
Stages of construction of the Tower of Pisa.

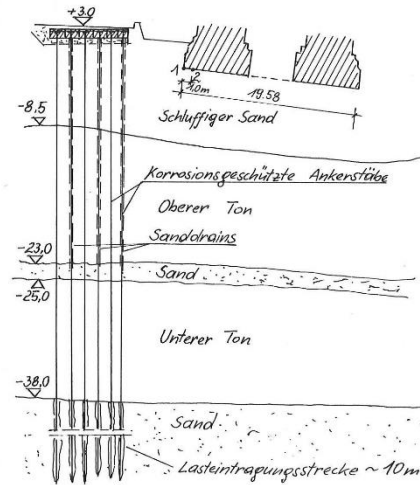


Abb. 4 N - S Schnitt
N - S section

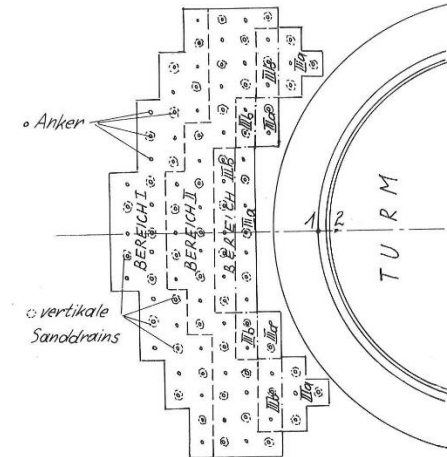


Abb. 2 Unterteilung des Ankerfeldes
Subdivision of the anchorage-field

nicht kleiner bzw. die maximale Kantenpressung nicht größer wird. Die Lastaufbringung erfolgt in Stufen von 0,5 bar, das entspricht etwa einer Ankerkraft von je 8,4 t. Für jede dieser

Source:

Ch. Veder: *Der schiefe Turm von Pisa. Bodenmechanische Probleme meines Sanierungsvorschlages*

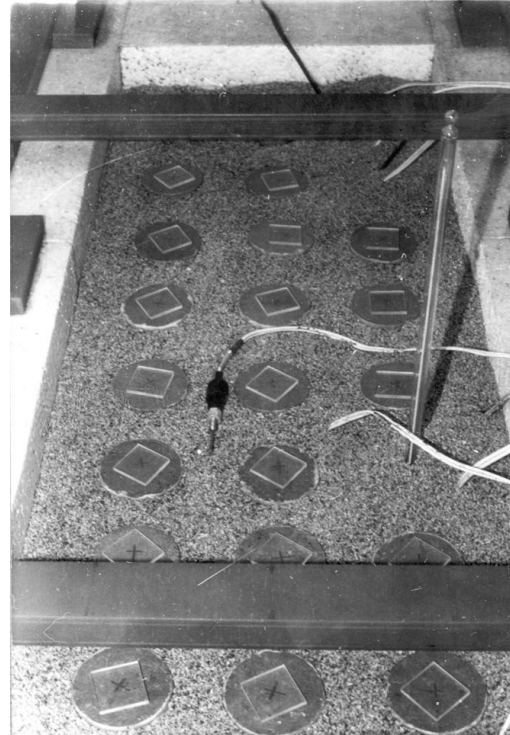
Technische Universität Wien - Mitteilungen für Grundbau, Bodenmechanik und Felsbau (1976)



- ISSMGE Vice-President for Europe 1997-2001
- President of Austrian Geotechnical Society 1972-2015
- Rankine Lecturer 2002
- Member of Royal Academy of Sciences of Belgium
- Member of New York Academy of Sciences
- Medal of Merit for Macedonia

Personalities: Heinz Brandl Professor at TU Wien 1981-2008

Laboratory experiments to investigate the effects of freezing-thawing cycles on the behaviour of lime and cement stabilized fine grained soils



Source:

H. Brandl: Der Einfluss des Frostes auf kalk- und zementstabilisierte feinkörnige Böden. Mitteilungen des Institutes für Grundbau und Bodenmechanik; Technische Hochschule (nunmehr Technische Universität) Wien, Heft 8, 1967

Innovative solutions for foundations of motorways in alpine regions in late 1970s (Tauernautobahn, Austria)

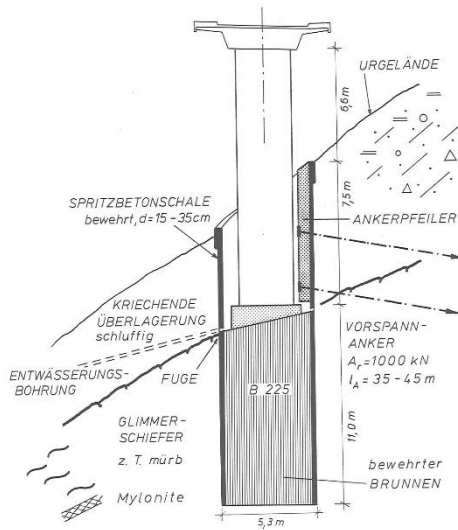


Bild 19:
Rampenbrücke L 22/1 (Betriebsumkehr Krems-
brücke): »Knopflochlösung« mit Ankerrippe in ellip-
tischem Spritzbetonschacht – Querschnitt

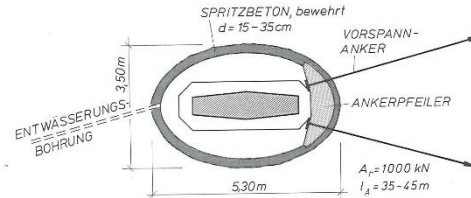
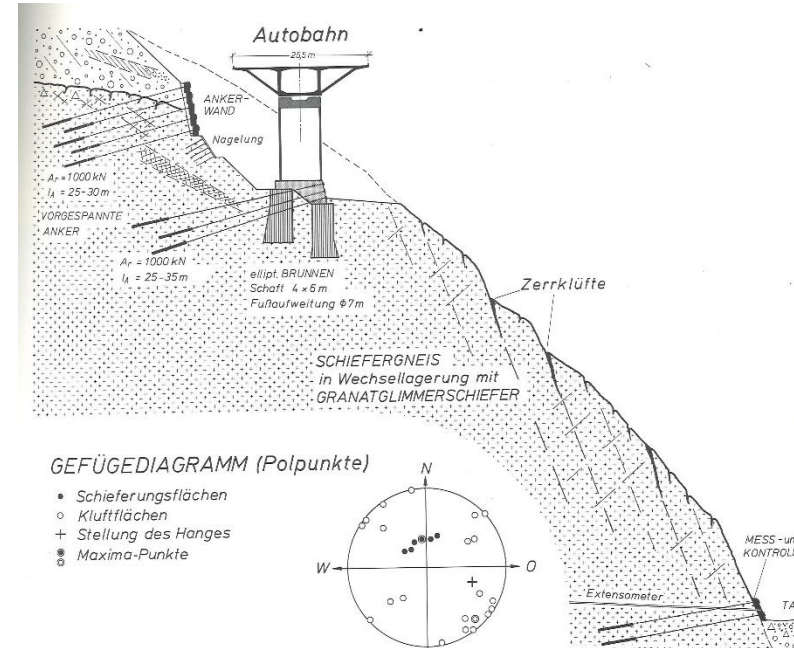
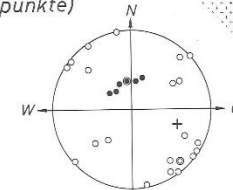


Bild 20:
Grundriß zu Bild 19



GEFÜGEDIAGRAMM (Polpunkte)

- Schieferungsflächen
- Klüffflächen
- + Stellung des Hanges
- ⊗ Maxima-Punkte



Source:

H. Brandl and H. Brandecker – Autobahnbau unter extremen geotechnischen Bedingungen
Technische Universität Wien - Mitteilungen für Grundbau, Bodenmechanik und Felsbau (1982)

Innovative solutions for foundations and slope stabilization of motorways in Austria



Source:

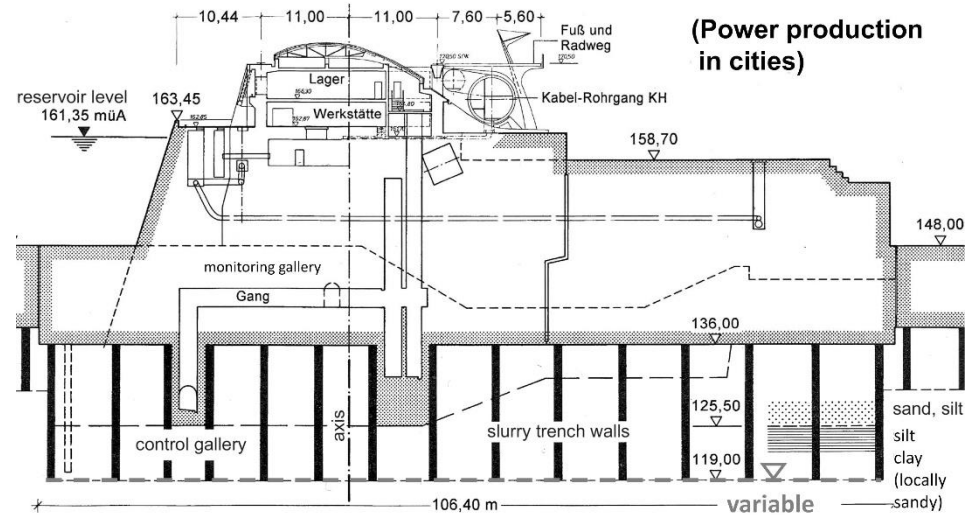
H. Brandl: Probleme des Erd- und Grundbaues bei der Tauernautobahn-Scheitelstecke.
Eigenverlag der Tauernautobahn AG, Salzburg, 1976



Source:

H. Brandl: Bridges, embankments and retaining structures in unstable slopes.
Keynote Paper. Conference „Contemporary Civil Engineering Practice 2012“. Faculty of Technical Sciences, University of Novi Sad and Society of Civil Engineers of Novi Sad, Serbia. 17-18 May, 2012. Proceedings, pp. 23 – 46.

Geotechnical Challenges at construction of power station Freudenau



Source:

H. Brandl: Bodenmechanische und erdstatische Fragestellungen beim Bau des Kraftwerkes Freudenau. Felsbau 15, Nr. 4. 1997

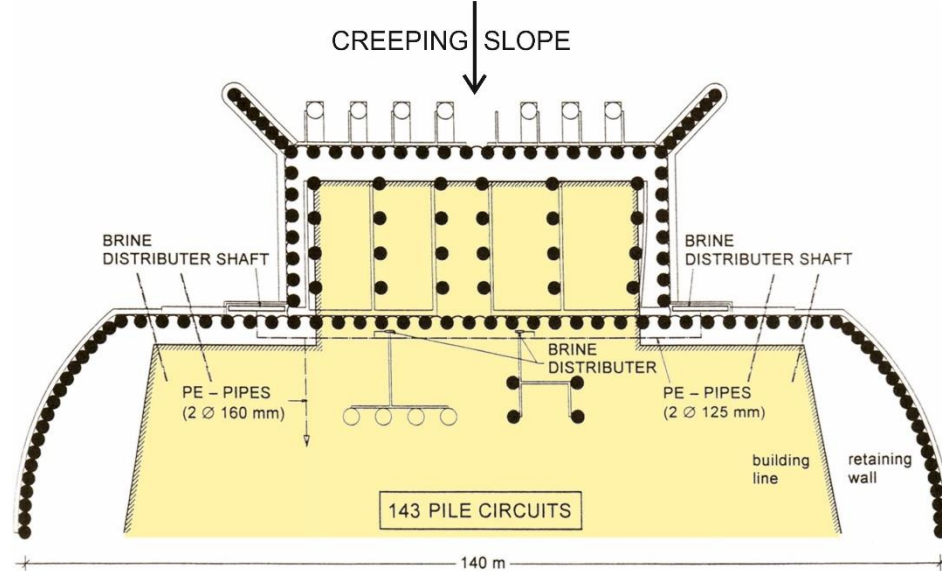
Reinforcement of 60 m high embankments (Egnatia Odos Highway, Greece)



Source:

H. Brandl: Geosynthetics applications for the mitigation of natural disasters and for environmental protection. Keynote Paper (extended "Giroud-Lecture" of IGS-World Conference in Brazil 2010) Geosynthetics International 2011, 18, No. 6 (Dec. 2011), pp. 340-390.

Innovative systems for energy foundations (Bad Schallerbach, Austria)



Source:

H. Brandl: Energy foundations for cooling and heating buildings (Innovative systems combining aspects of construction, energy and environmental protection). 25th Anniversary of the Austro-Arab Chamber of Commerce (AACC) Vienna, 22 May, 2014

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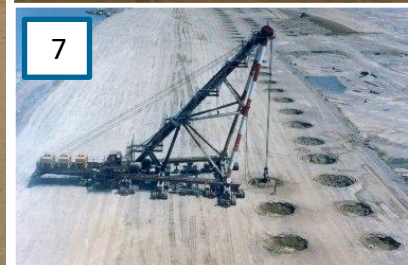
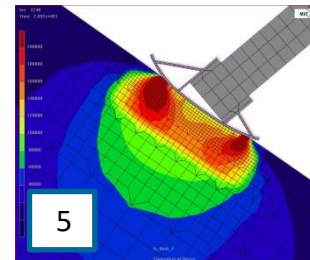
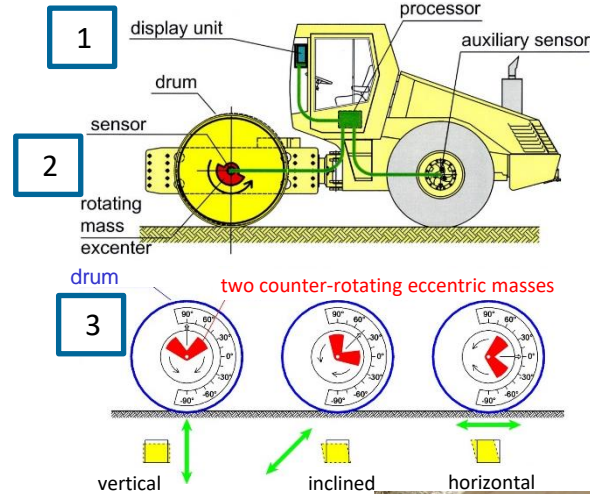
■ Miscellaneous

- International Projects of Specialist Contractors
- Young Member Presidential Group
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- Bid for 21st ICSMGE 2026 in Vienna

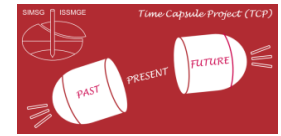
PAST

FUTURE

1. Continuous Compaction Control (CCC) with vibratory rollers
2. CCC for various types of excitation
3. Control criteria and compaction optimization for feedback controlled rollers
4. Compaction effect of dynamically excited polygonal drums
5. Equipment optimization for vibratory plates and roof compactors
6. Compaction effect and documentation of Rapid Impact Compaction
7. Integrated compaction control for dynamic compaction
8. Dynamic load plate test with the falling weight deflectometer and calibration of the dynamic load plate



Time Capsule Project (TCP)



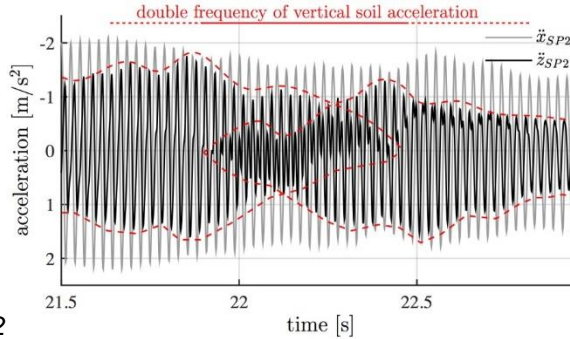
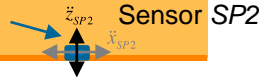
26

Research TU Wien: Development of an IC System for Oscillation Rollers

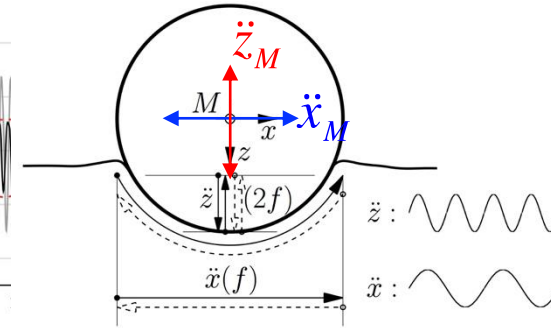
The forwards-backwards rotation of an oscillating drum ... causes a characteristic behaviour of soil accelerations ... due to the settlement trough.



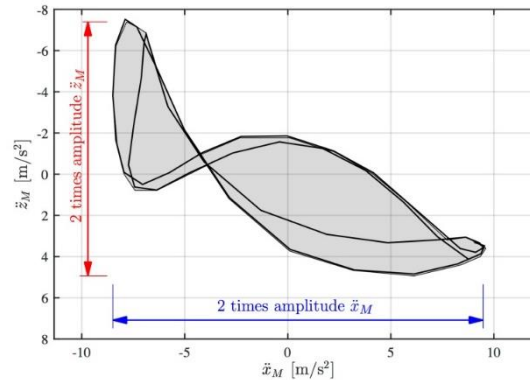
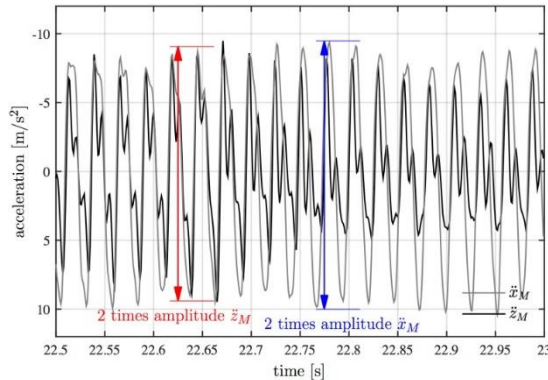
Pistol, Villwock, Völkel,
Kopf & Adam, 2016



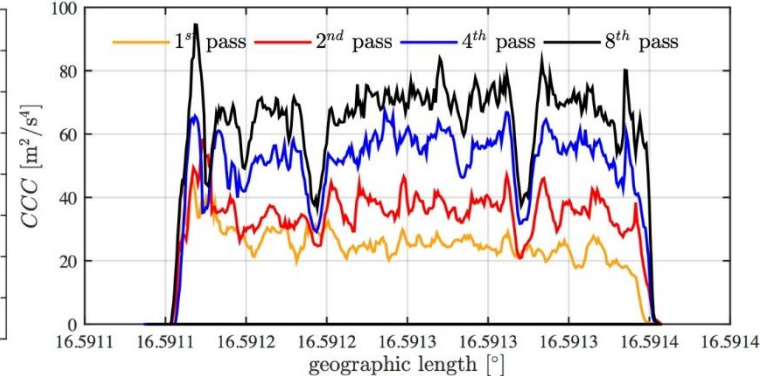
Soil accelerations measured by Sensor SP2



The characteristics replicate the bearing of the drum (point M) ...



... and are used in an algorithm to calculate the first functional ICMV (CCC value) for oscillation rollers:

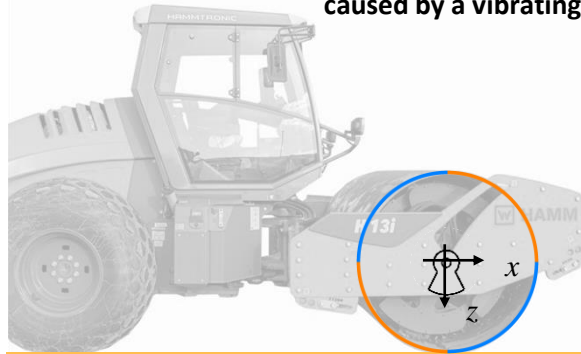


Research TU Wien: Development of a novel ICMV for Vibratory Rollers

The mainly vertical loading of the subgrade
caused by a vibrating drum ...

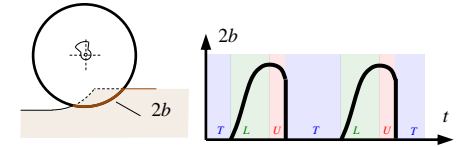
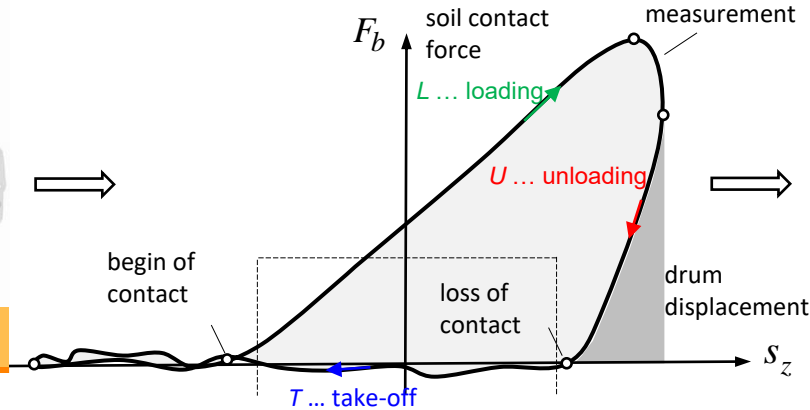
... results in a measured soil response
(force-displacement diagram):

The measured motion behavior of
the drum gets applied to a
simplified model ...



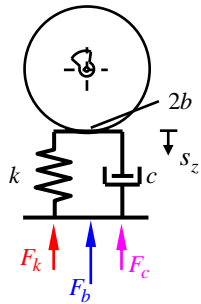
Hager, Pistol, Kopf & Adam, 2021

F_b

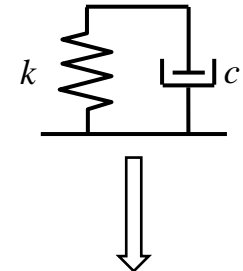
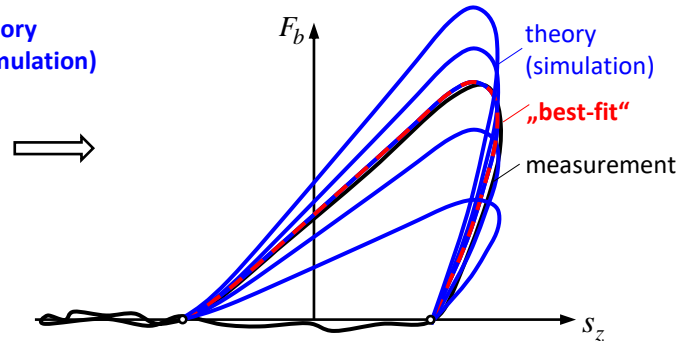
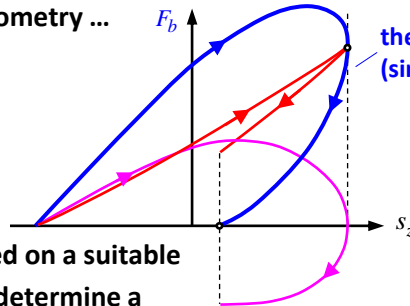


... to determine the contact
geometry between the drum
and the subgrade:

The measured motion behavior
with the corresponding contact geometry ...

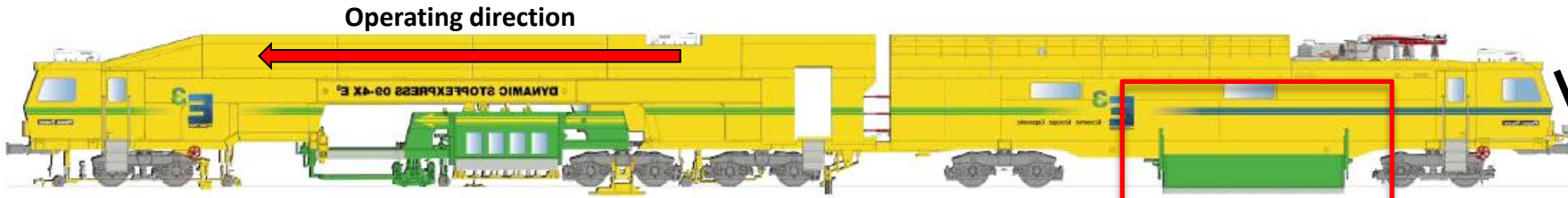


... gets imposed on a suitable
soil model to determine a
theoretical system response.



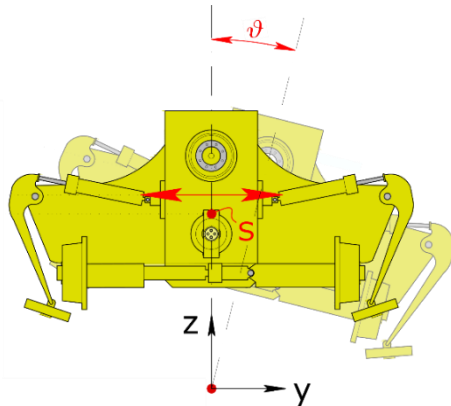
$$k = f(E)$$

Research TU Wien: Ballast Compaction with the Dynamic Track Stabilizer

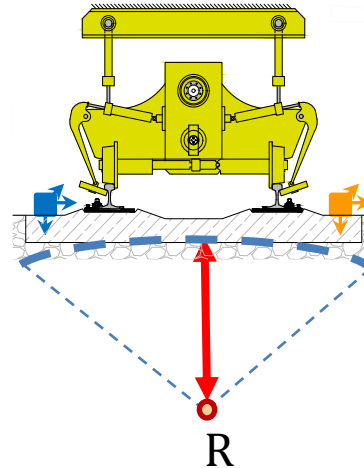


Alignment/Tamping

The design of the DTS causes a rocking motion ...

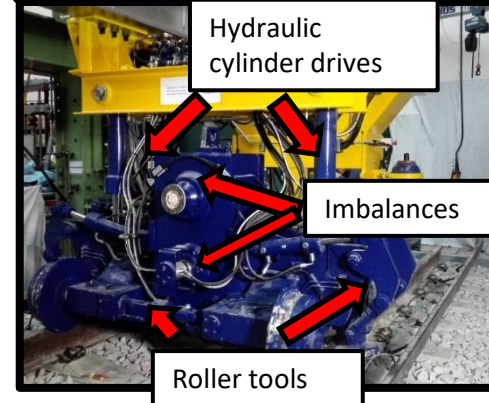


Barbir, Pistol, Kopf, Adam, Auer & Antony, 2019



... which can also be observed on the sleepers.

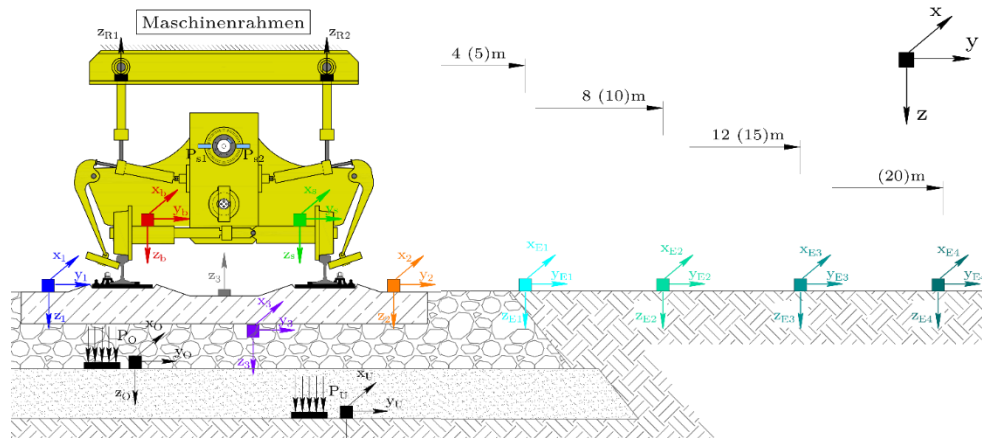
Dynamic Track Stabilizer



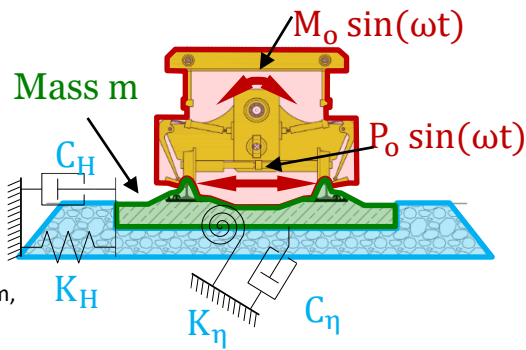
Components of the DTS

Research TU Wien: Modelling the Machine-Soil Interaction

A unique measurement setup ...

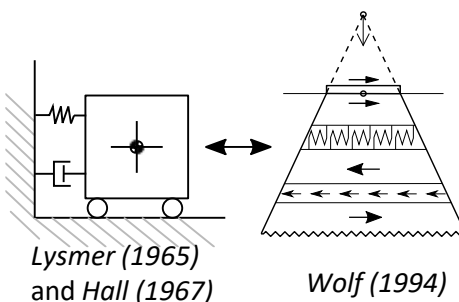
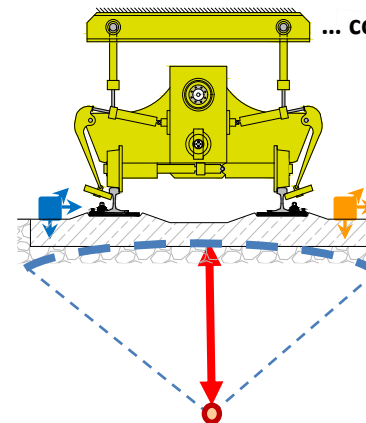


... lead to a (verified)
simple mechanical
model ...

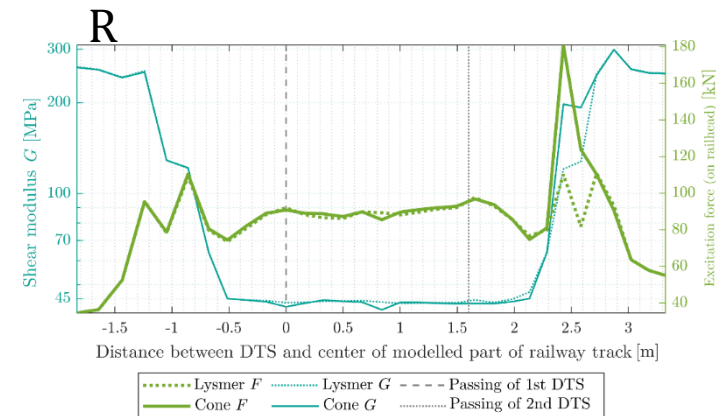


Dafert, Pistrol, Kopf & Adam,
ongoing research

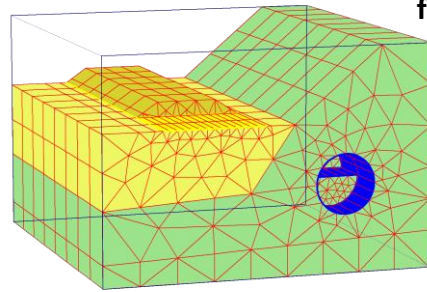
... combined with simplified kinematics ...



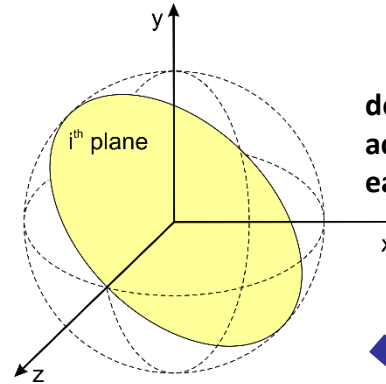
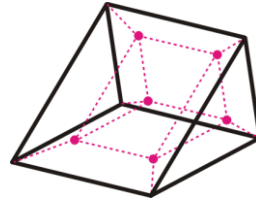
... which allows for the
back-calculation of soil
parameters (like shear-
modulus G):



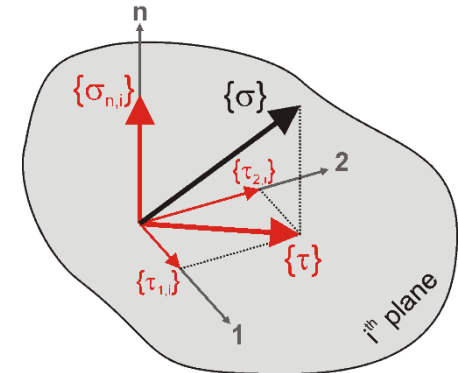
Basic Formulation



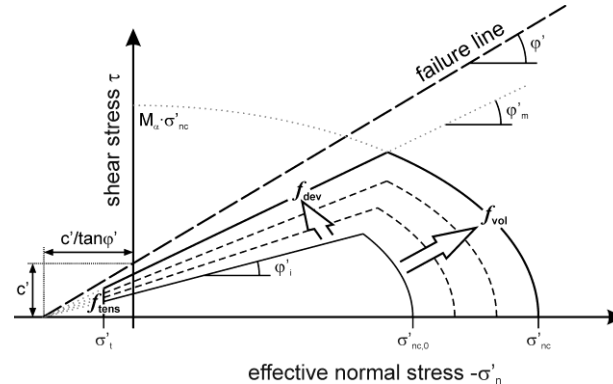
finite element



definition of n independently
acting integration planes in
each stress point



calculation of local stress components
from global stress state



formulation of constitutive
relations on integration planes

$$d\varepsilon = \sum_{i=1}^n T_i \cdot d\varepsilon_i \cdot w_i$$

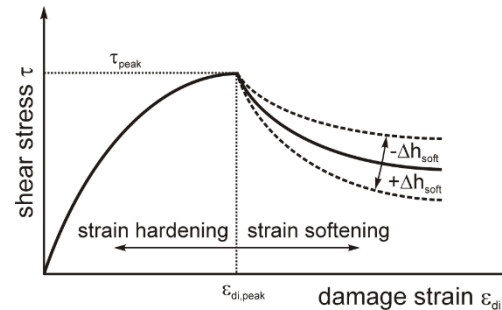
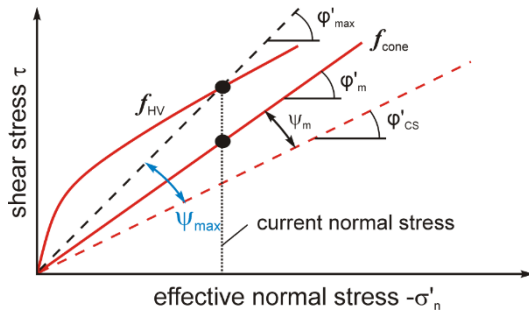
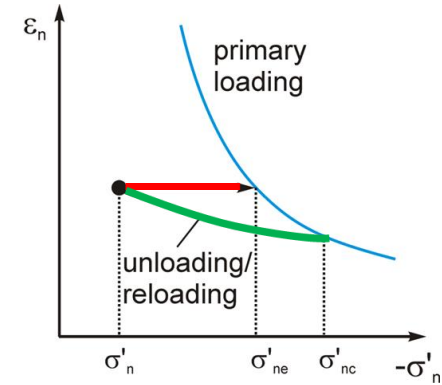
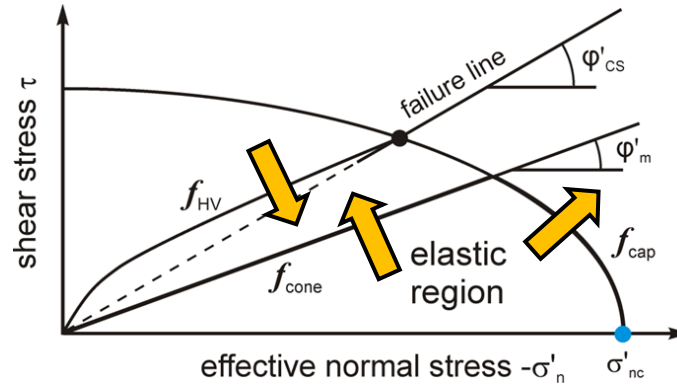
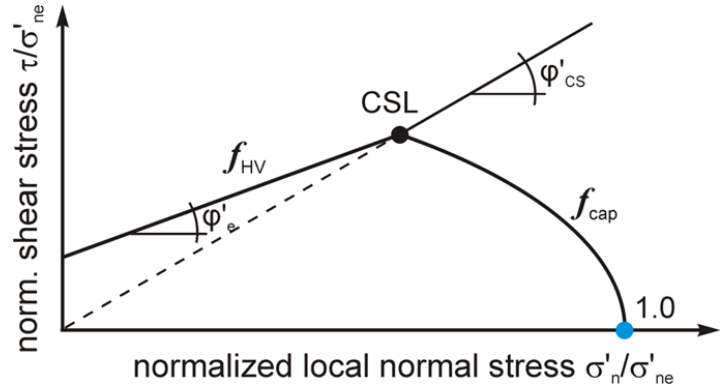
weighted summation over
all integration planes
> global behaviour



Enhancement

Hvorslev-Surface for OC-Soils

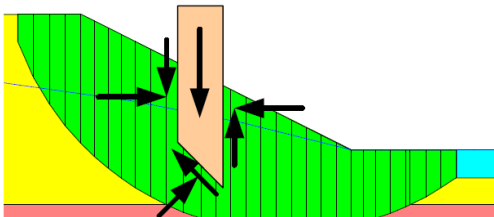
- Local stresses τ , σ'_n and local normal strains ε_n



- Plastic normal strains reduce pre-consolidation pressure σ'_{nc}
- Softening parameter h_{soft} governs rate of strain softening

Research Graz University of Technology: Slope Stability Analysis [FELA / SRFEA]

Limit Equilibrium Analysis



- Overall form of the failure surface needs to be determined in advance
- Distribution of the interslice forces is assumed differently in various methods
- Kinematic admissibility is not ensured
- Need to perform a global search for identifying the failure mechanism with the lowest factor of safety

Finite Element Limit Analysis (FELA)

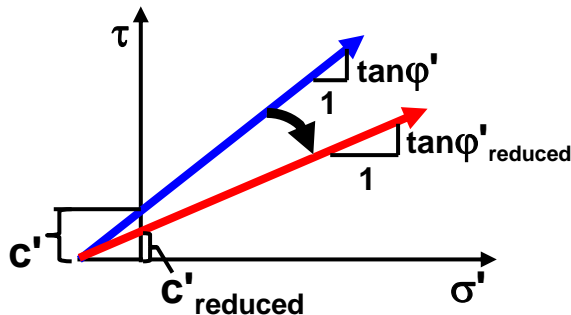
Lower bound

- Requires a stress field that satisfies the **boundary conditions**, the **yield criterion** and fulfils **equilibrium**.
- Any loads supported by such a stress field are a lower bound on the true failure load.

Upper bound

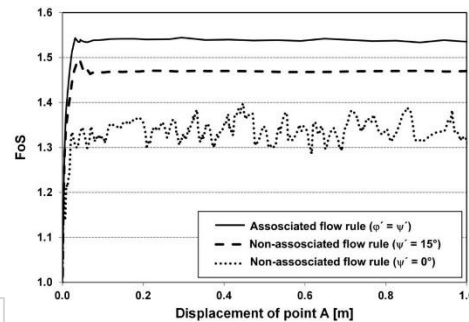
- Is based on a velocity field that satisfies the **boundary conditions** and implies an **associated flow rule** (strain and velocity compatibility conditions).
- **Internal work** (due to plastic shearing) is equated to the **external work** (minimum internal power dissipation).
- Any loads derived from such a velocity field are an upper bound on the true failure load.

Strength Reduction Finite Element Analysis



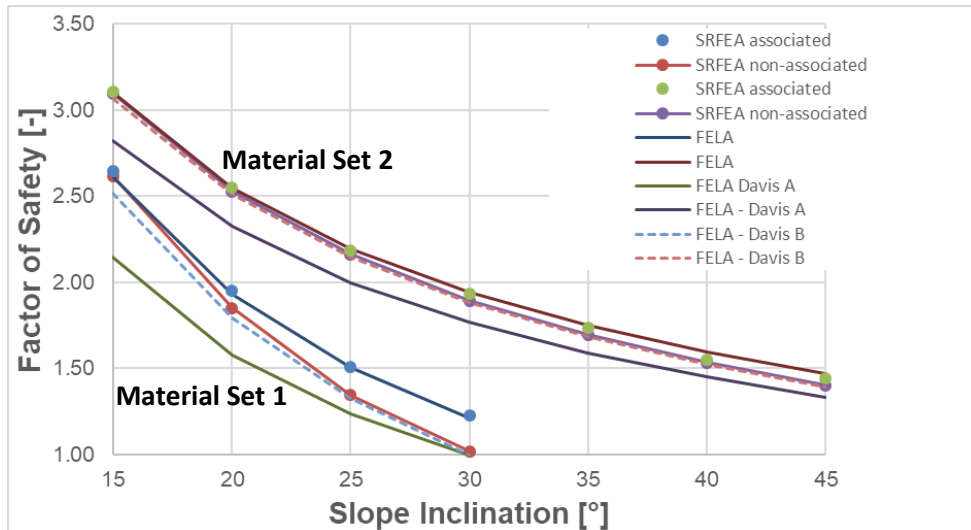
$$FoS = \frac{c'}{c'_{reduced}} = \frac{\tan \phi'}{\tan \phi'_{reduced}}$$

- **Disadvantage FELA:** implies associated plasticity
- **Disadvantage SRFEA:** non-associated plasticity may lead to numerical instabilities

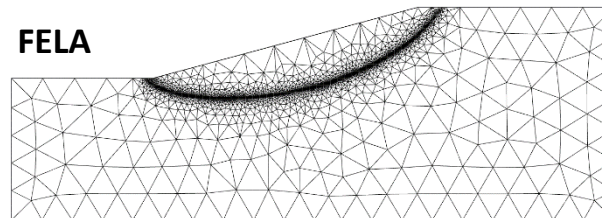


**Possible solution:
Modified “Davis-
Approach”**

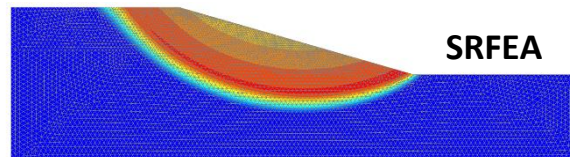
Example:



FELA



SRFEA



Research Graz University of Technology: Characterization of structured sediments

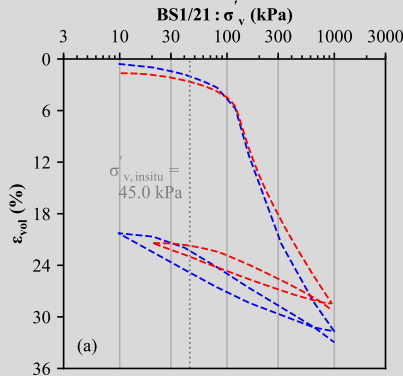
Parameter identification by means of in-situ & laboratory tests

Aim: Improved characterization of **stress-strain behavior** in postglacial sediments using **CPTu & SDMT**

Basis: Test sites



Post glacial sediments: Fussach, Salzburg & Seekirchen



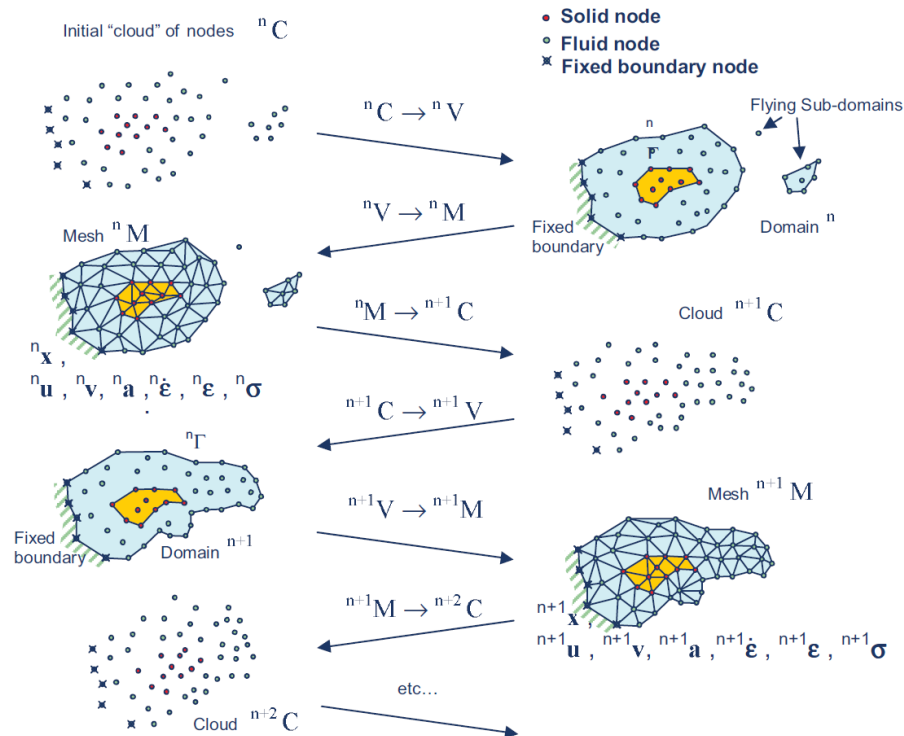
Young sediments:
Water reservoir Raggal

- (1) Execution of **CPTu & (Medusa) SDMT**
- (2) **Soil sampling** (e.g. block sampling) for laboratory testing
- (3) Comprehensive **laboratory investigations** on undisturbed & reconstituted soil samples (e.g. bender element)

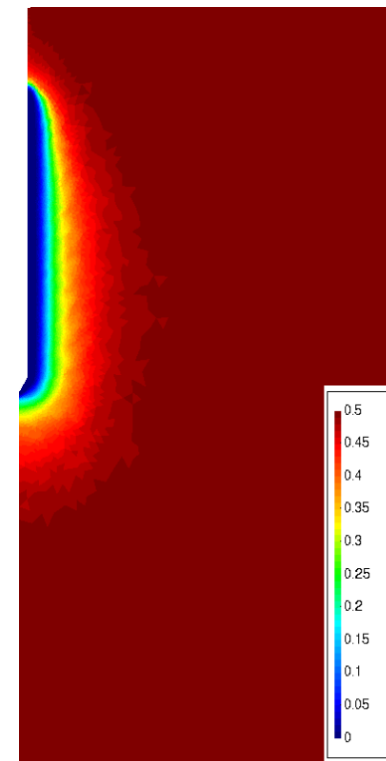
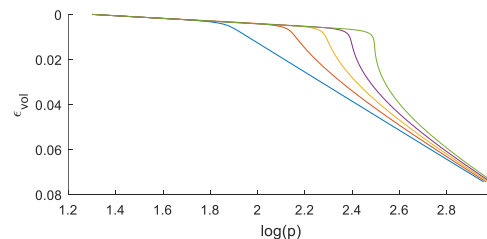
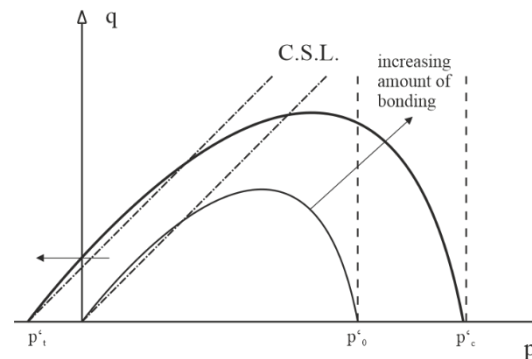
Interpretation:

Development of new **correlations** for CPTu & SDMT, calibrated based on laboratory results & monitoring data

Particle Finite Element Method



Constitutive Model: CASM including destructuration

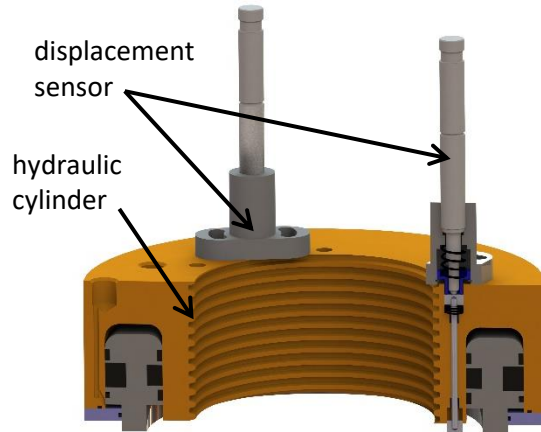
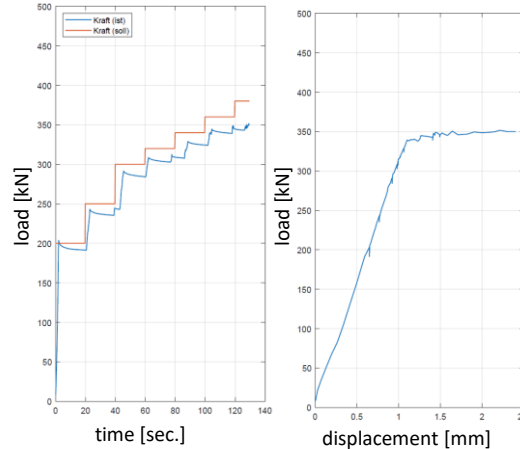


Example: Zone of destructuration during penetration

Research Graz University of Technology: Anchor lock-off-testing

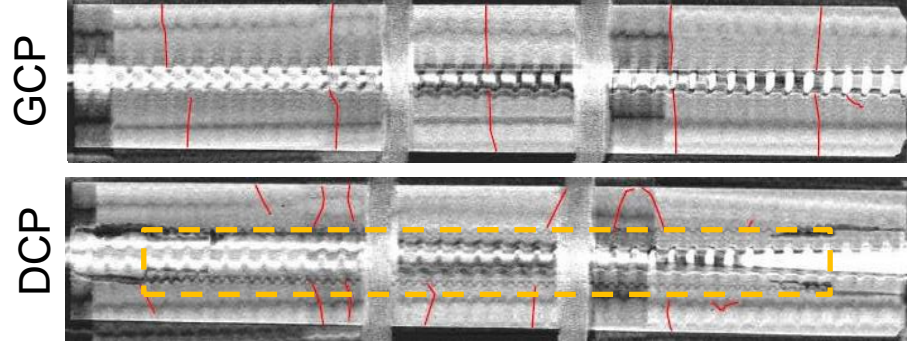
Anchor lock-off-testing

- Determination of the lock-off-load
- Smaller and smarter equipment for anchor testing
- Changes in lock-off-load or behaviour of the anchor during the test give a feedback on damages or damage symptoms

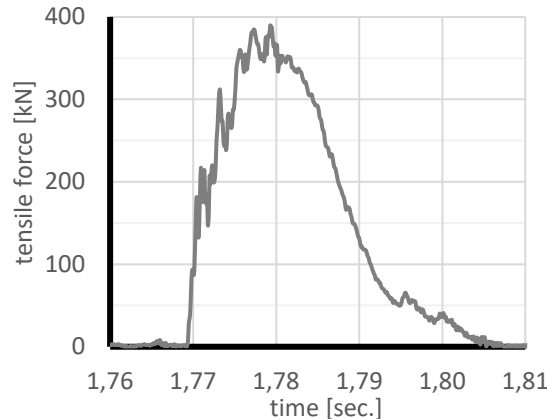


Research Graz University of Technology: Durability of micro-piles

CT-Imaging of cracked grout bodies



Dynamic testing of micro-piles



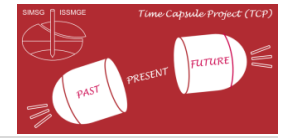
Durability of micro-piles for natural hazard protection

CT-imaging

- Grout cover protection (GCP) as a main corrosion protection system
- Corrosion of the (metal) tensile element due to a cracked grout body
- Crack width and distribution unknown
- Cracking behaviour influenced by corrosion protection systems (e.g. double corrosion protection DCP)

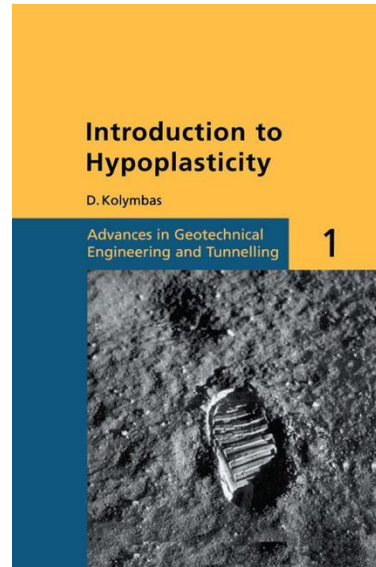
Dynamic loading vs. static loading

- Dynamic impacts due to natural hazard protection (e.g. rockfall)
- Static testing complex, cost-intensive and not corresponding to realistic loading effects (e.g. dynamic impact)

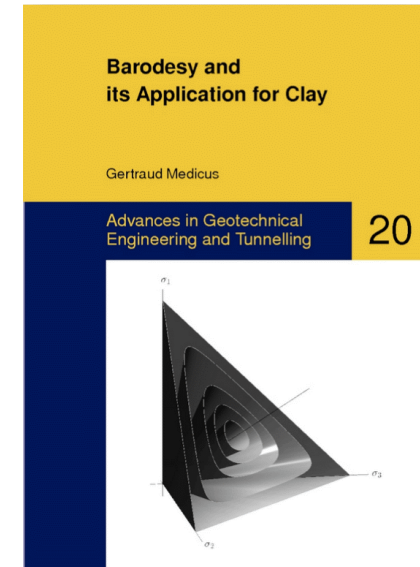


Developing of alternative constitutive models for soils, i.e. models without yield surface and no splitting of strain in elastic and plastic part

Hypoplasticity



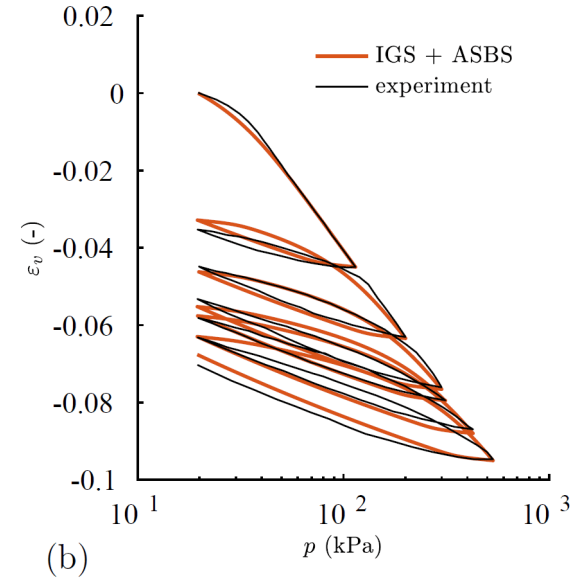
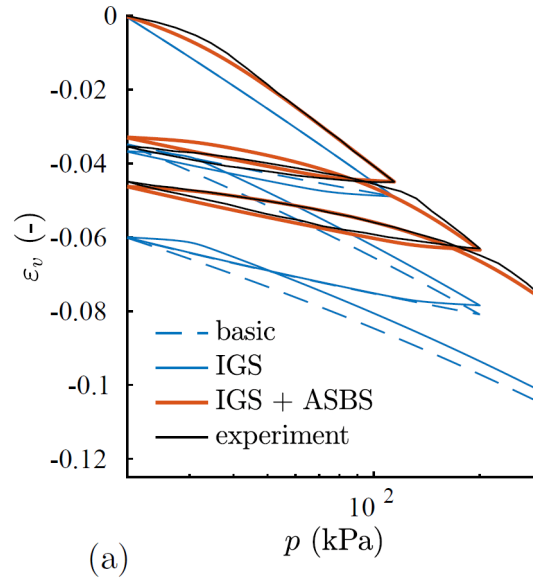
Barodesy



Originated in 1985 by D. Kolymbas in Karlsruhe with major contributions since 1997 in Innsbruck in numerical implementation by D. Roddemann, W. Fellin, A. Ostermann

Originated in 2009 by D. Kolymbas in Innsbruck with contributions of G. Medicus, W. Fellin, M. Bode, A. Ostermann

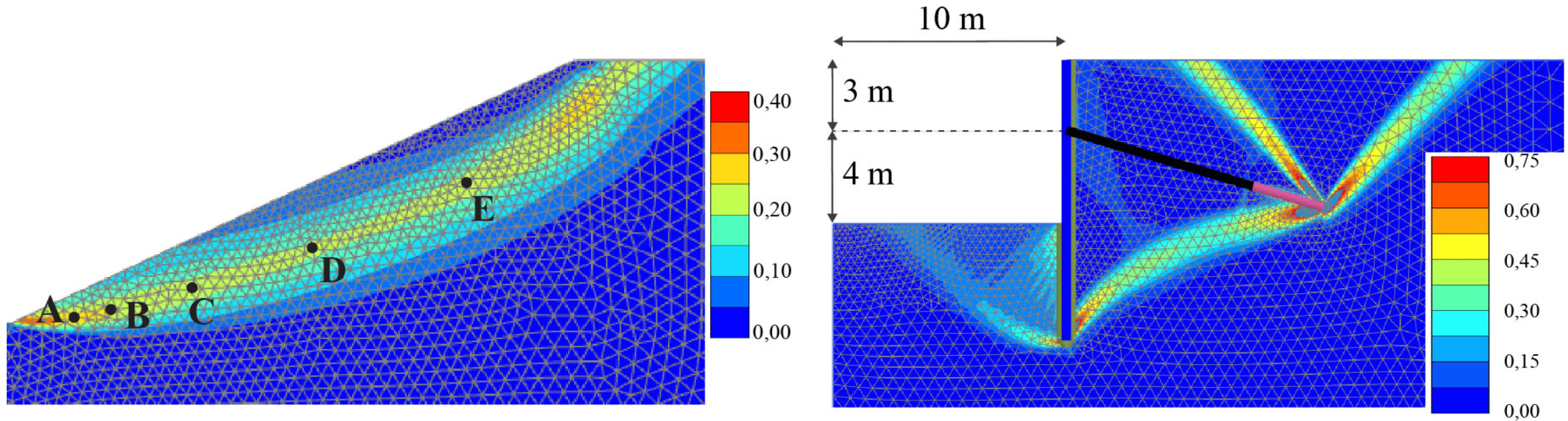
Enhancing the numerical response to cyclic loading



Cyclic oedometer test: Experiments on reconstituted Newfield clay by D. Namy (1970); IGS ... intergranular strain concept by Niemunis & Herle (1997), ASBS ... asymptotic boundary surface extension by M. Bode & W. Fellin & G. Medicus (2021)

Applying strength reduction to non-elasto-plastic models

(B. Schneider-Muntau & G. Medicus & W. Fellin, 2018)



Shear zones at failure indicated by void ratio; Barodesy implemented in Plaxis

(M. Bode & G. Medicus & W. Fellin, 2020)

Numerical Modelling of debris flow and snow avalanches



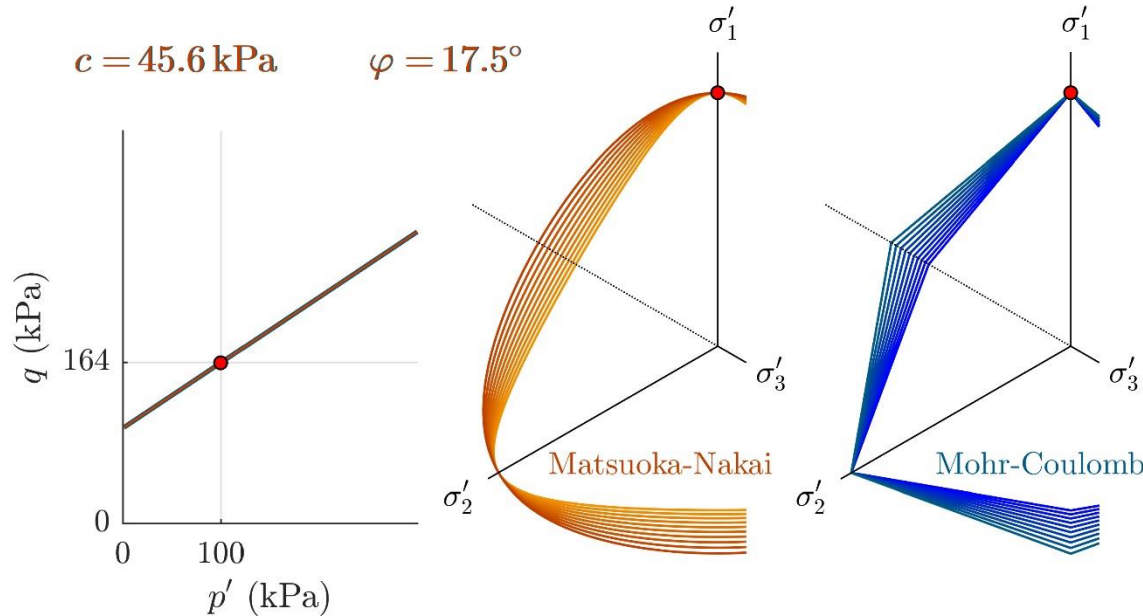
[Video](#) of simulation

Tsunami modelling of the 2014 Lake Askja flank collapse ([Rauter et al., 2022](#))
computed on the High Performance Computing cluster at the University of Innsbruck

Research University of Innsbruck: Teaching and Learning Constitutive Models

Open education project: <https://soilmodels.com/soilanim/>

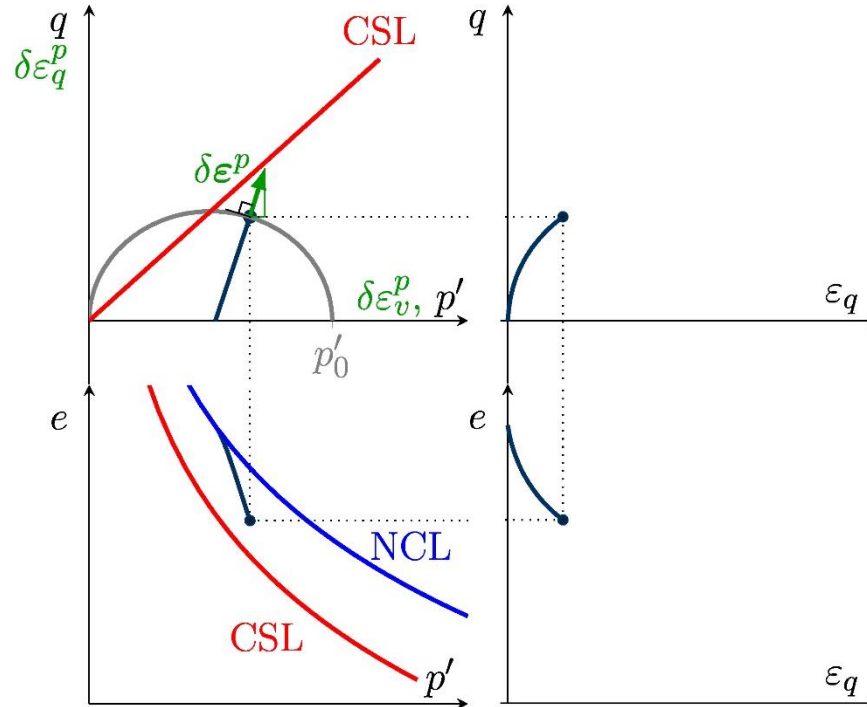
Matsuoka-Nakai vs. Mohr-Coulomb: [\[click to start animation\]](#)



How does c and φ affect strength predictions?
(keeping one axisymmetric stress state ●)

Modified Cam Clay Model: [\[click to start animation\]](#)

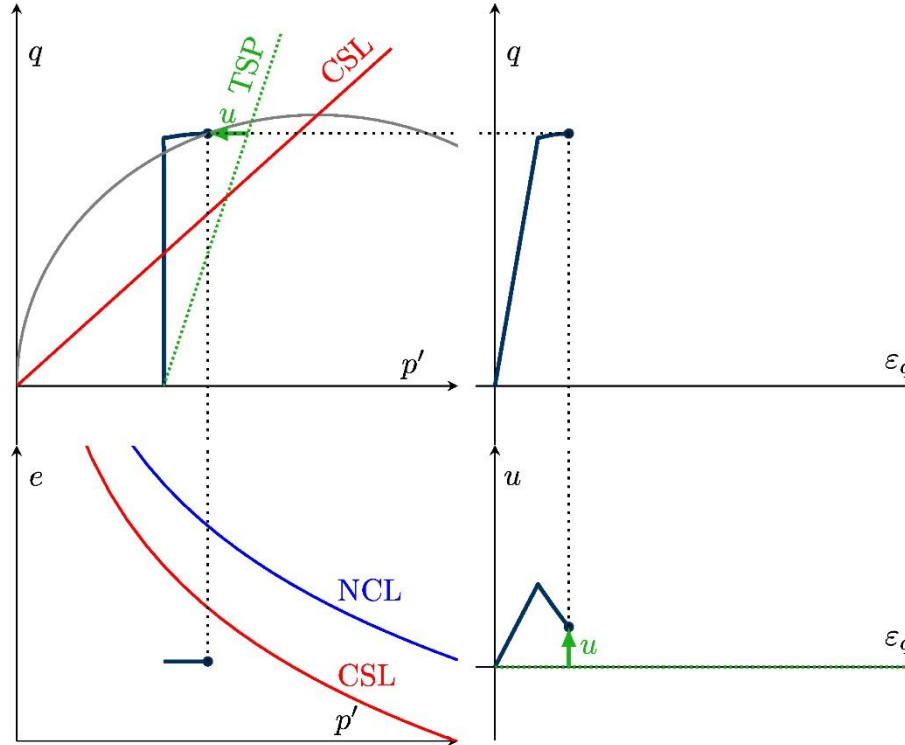
Conventional,
drained triaxial test,
normally
consolidated



MCC Model (Roscoe & Burland, 1968):
Drained triaxial test of normally consoli-
dated clay

Modified Cam Clay Model: [\[click to start animation\]](#)

Conventional,
undrained triaxial test,
Highly
overconsolidated



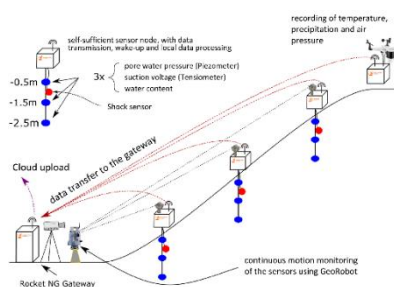
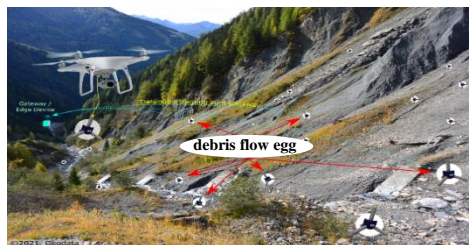
MCC Model (Roscoe & Burland, 1968): Undrained triaxial test of highly overconsolidated clay



Gertraud Medicus

HangmurenNet

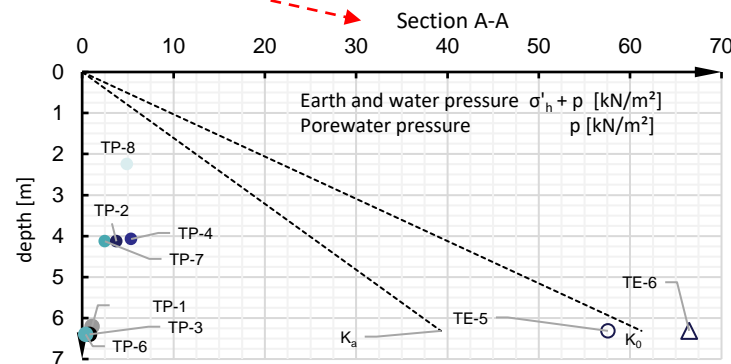
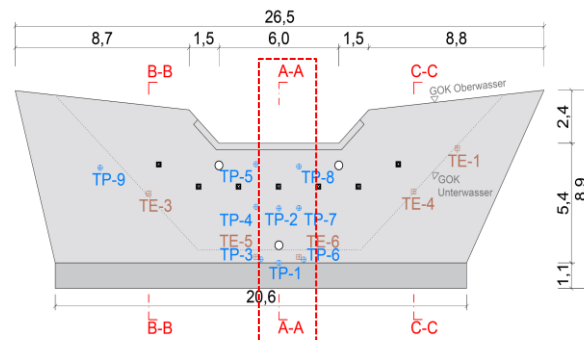
- Measurement of relevant (hydro)geological parameters and characteristics of the slope debris flow
- Continuous measurement of possible trigger parameters on/in the slope debris flow



Hofmann, Berger, Wimmer (2021)

Water pressure on torrent barriers

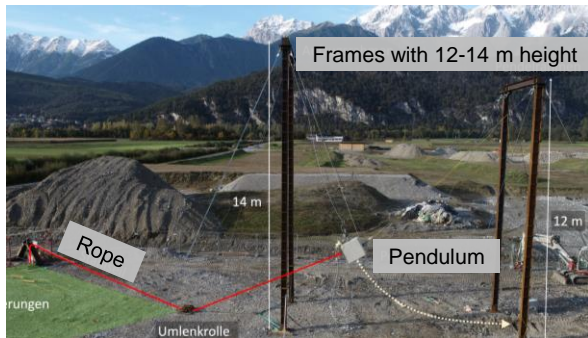
- Measurements on different barriers with piezometer and earth pressure cells in Tirol



Hofmann, Berger, Steinwender & Wimmer (2022)

Foundations of rockfall protection fences

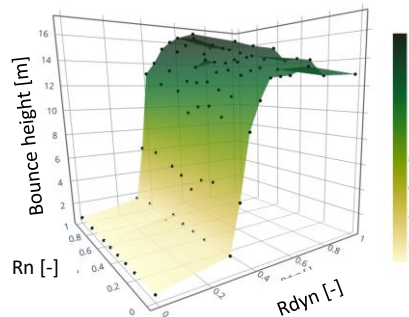
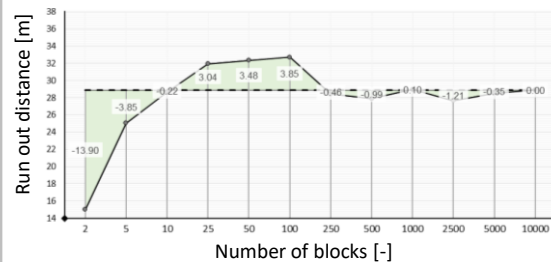
- Impact loading on micropiles and post foundations
- 100 field test on micropiles and foundation



Hofmann, Wimmer, Berger & Steinwender (2020)

Rockfall simulations - convergence and sensitivity analysis - for design of foundations

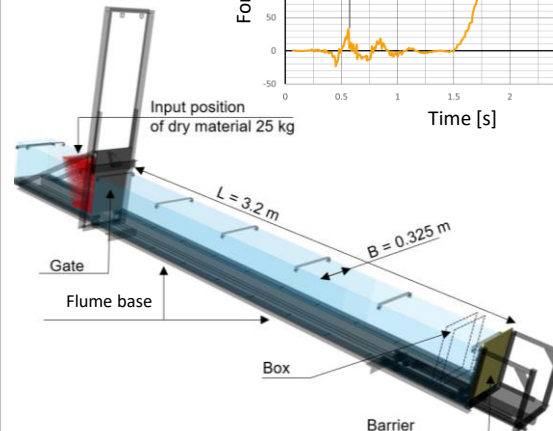
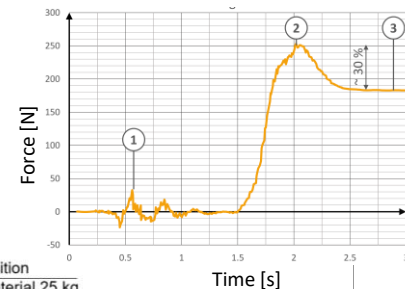
- Determination of run-out distances and bounce heights (sensitivity analysis)



Hofmann, Berger (2021)

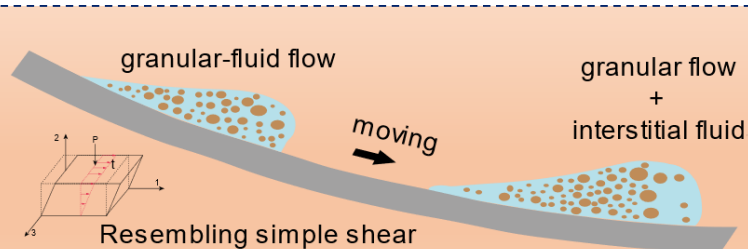
Impacts on barriers by flow-like gravitational mass movements

- 180 model test with different materials and barriers
- Back-calculation of the results from the model test with numerical simulations



Hofmann, Berger & Wimmer (2020)

Research BOKU: Constitutive Model for Granular Flows with Interstitial Fluids



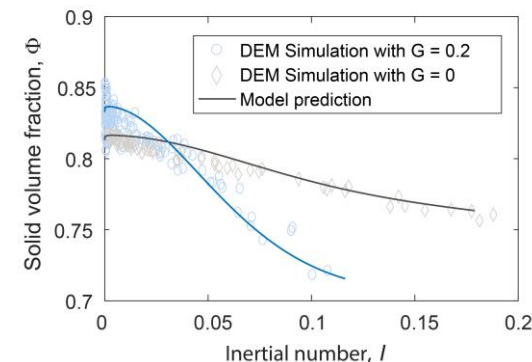
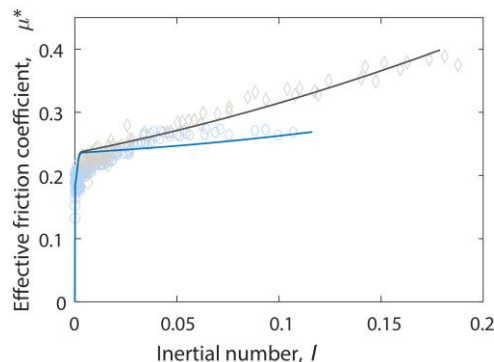
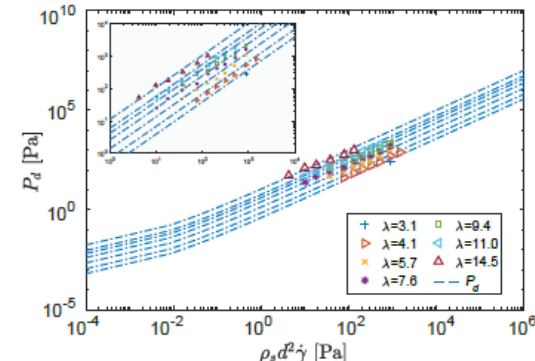
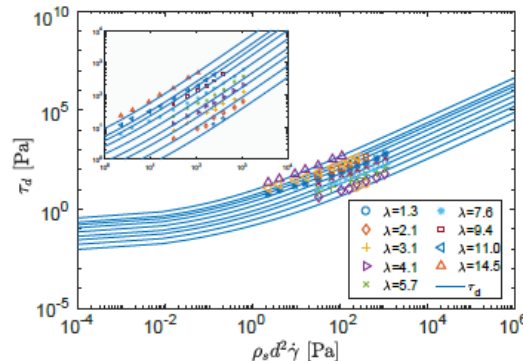
- Solid concentration significant affect dynamic behaviour
- Normal stress effect

Model framework

$$\dot{\mathbf{T}} = \dot{\mathbf{T}}_{\text{hypo}} + \dot{\mathbf{T}}_{\text{dynamic}}$$

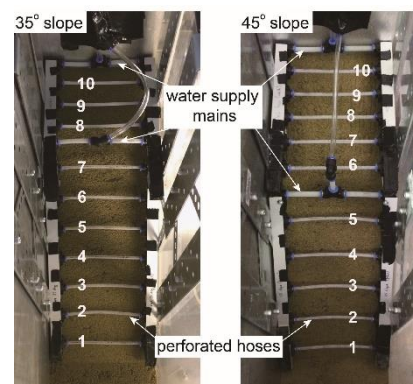
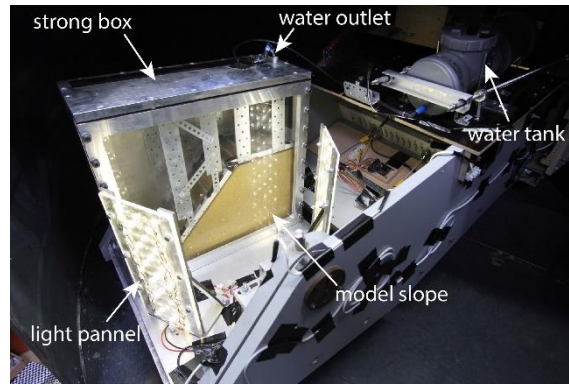
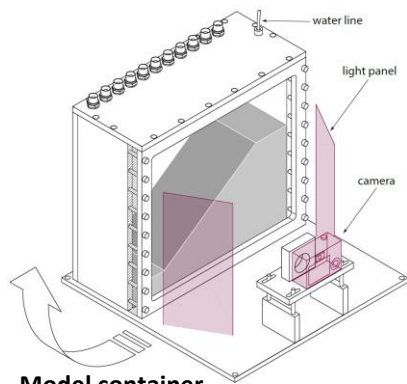
Model equation

$$\dot{\mathbf{T}} = f_s \left[(\text{tr} \mathbf{T}_h) \mathbf{D} + f_v (\text{tr} \mathbf{D}) \mathbf{T}_h + a^2 \frac{\text{tr}(\mathbf{T}_h \mathbf{D})}{\text{tr} \mathbf{T}_h} \mathbf{T}_h + f_{da} (\mathbf{T}_h + \mathbf{T}_h^*) \|\mathbf{D}\| \right] + \underbrace{(2K_1 + 4K_2 \|\mathbf{D}\|) \dot{\mathbf{D}}}_{\text{shear stress}} - \underbrace{\frac{4K_2}{\tan \alpha_i} (\mathbf{D} \dot{\mathbf{D}} + \dot{\mathbf{D}} \mathbf{D})}_{\text{normal stress}}$$



Comparison between model prediction and DEM simulations (Cruz et al. 2005) of dry dense granular flow in simple shear tests

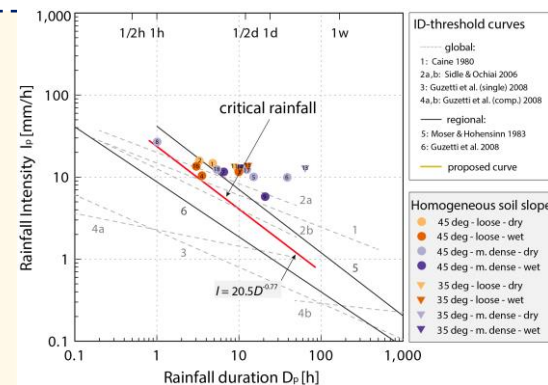
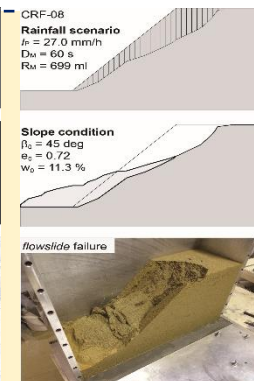
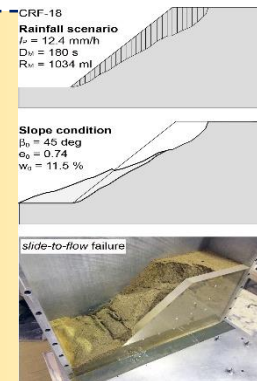
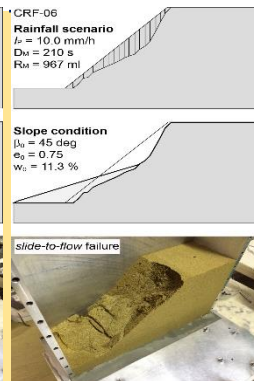
Research BOKU: Centrifuge Modelling of Rainfall-Induced Slope Failure



The roles of rainfall intensity and initial conditions, such as slope angle, porosity and degree of saturation of the soil, in the failure initiation and post-failure kinematics are considered.

Centrifuge model with the rainfall system

Most of the slopes exhibit a flow-type failure pattern, either following the slide-to-flow or the flowslide failure modes.

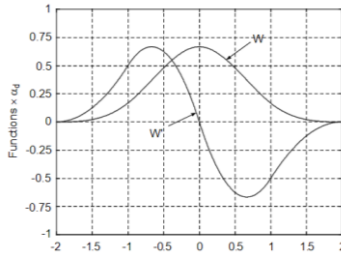
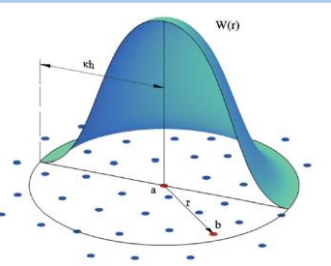


Failure patterns under varying rainfall intensity

ID threshold curves

Research BOKU: Landslide Modelling with Smoothed Particle Hydrodynamics (SPH)

- Lagrangian particle-based method for convenient simulations of large deformations
- Various constitutive models for different material behaviours
- Massive GPU parallelization for large-scale modeling



Support domain and kernel function

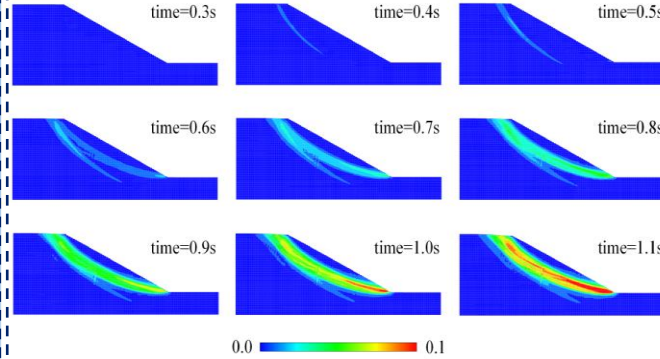
SPH forms of governing equations

$$\frac{D\rho_i}{Dt} = \sum (\mathbf{v}_i - \mathbf{v}_j) \cdot \nabla_i W_{ij} m_j \quad \frac{D\mathbf{v}_i}{Dt} = \sum \left(\frac{\sigma_i}{\rho_i^2} + \frac{\sigma_j}{\rho_j^2} \right) \cdot \nabla_i W_{ij} m_j + \mathbf{f}_i$$

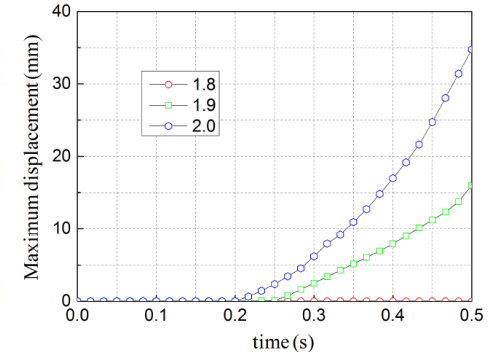
Constitutive models

Hypoplastic models

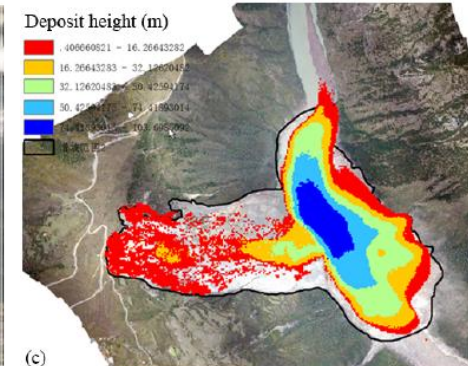
Elastoplastic/Viscoplastic models



Development of failure surface

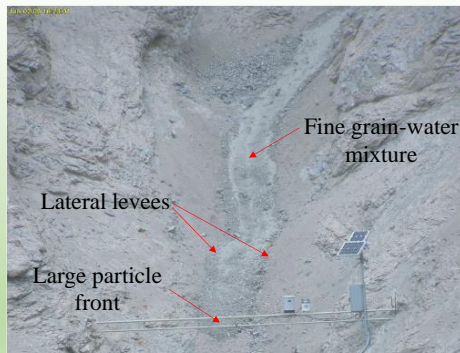


Evaluate the factor of safety

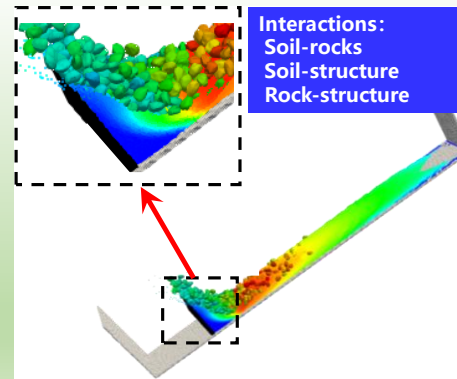


Three-dimensional large-scale modelling of Baige landslide

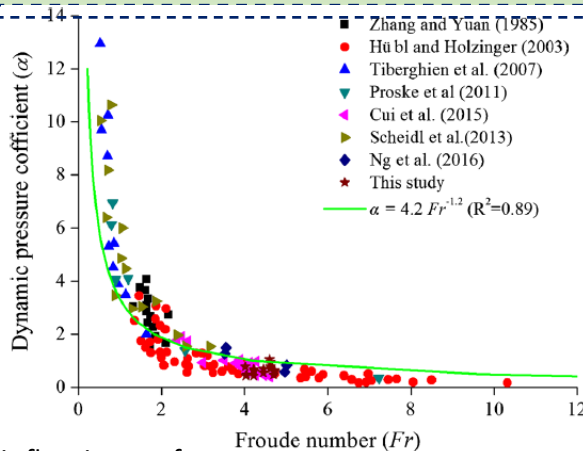
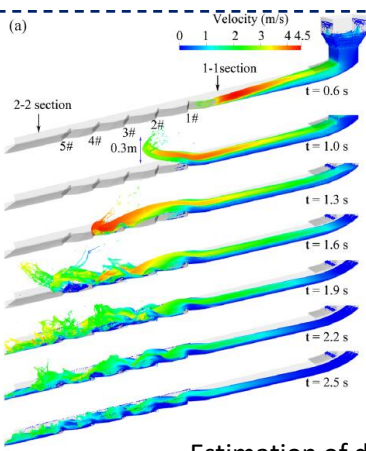
Research BOKU: Single Phase and Multiscale Modelling of Debris Flows (SPH-DEM)



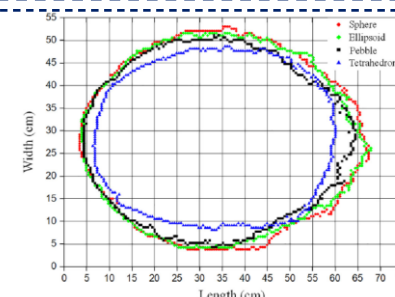
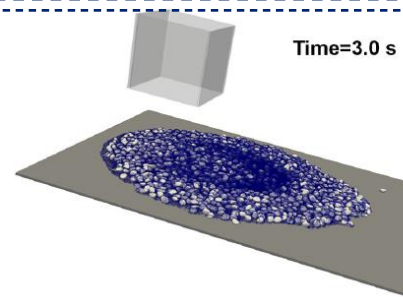
Multiscale phenomena: particle segregation interaction with structures



- A resolved SPH-DEM method for the multiscale modeling of debris flow
- DEM to consider arbitrarily complex rock shape
- SPH with elastoplastic/viscoplastic models for the continuous phase



Estimation of debris flow impact forces



- Coupled modeling shows the strong impact of particle shape in debris materials
- Segregation and impact with structures can be modelled

Content

■ Personalities

- Karl von Terzaghi
- Christian Veder
- Heinz Brandl

■ Past and Current Research Activities

- TU Wien (TUW)
- Graz University of Technology (TUG)
- University of Innsbruck (UIBK)
- University of Natural Resources and Life Sciences, Vienna (BOKU)

■ Miscellaneous

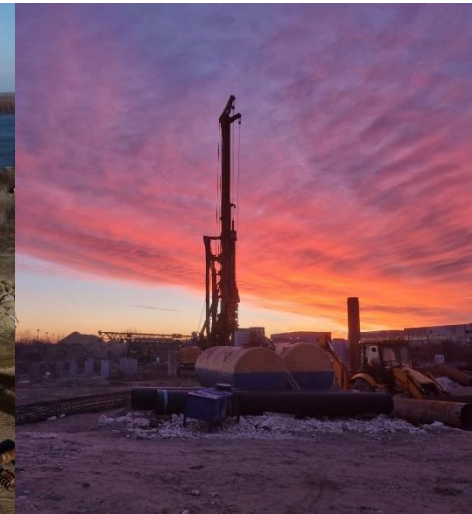
- International Projects of Specialist Contractors
- Young Member Presidential Group
- Conferences
- Bid for 21st ICSMGE 2026 in Vienna

PAST

FUTURE

■ Silo Yard Silistra Project, Bulgaria

- Execution of modern silos storage facilities with capacity of over 350,000 m for the leading company in the field of agricultural production and processing of grains and seeds (non-GMO; non- heavily treated crops) in Bulgaria
- Drilling of over 1,000 foundation piles with diameter 88 cm
- Construction period: 10/2021 – 10/2022



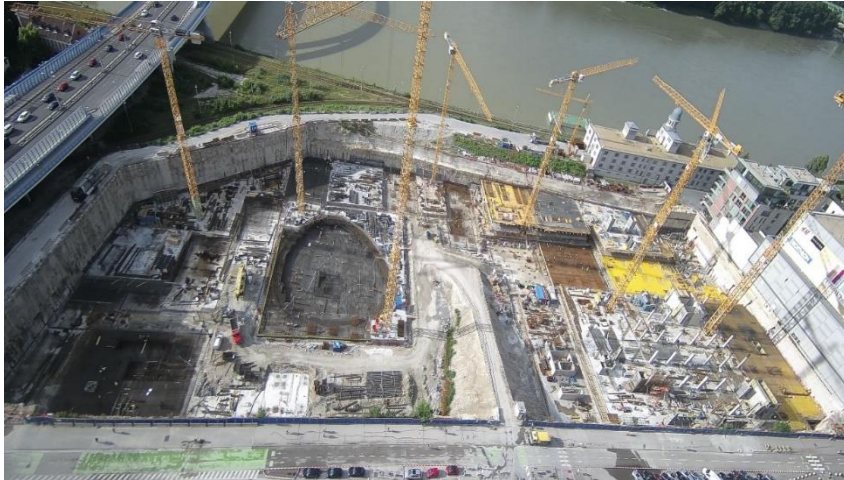
- **Bem Palace, Budapest, Hungary**
- Deep excavation: slurry walls 40 cm thickness, 3 rows of anchors and struts
- Construction period: 02/2021 – 02/2022



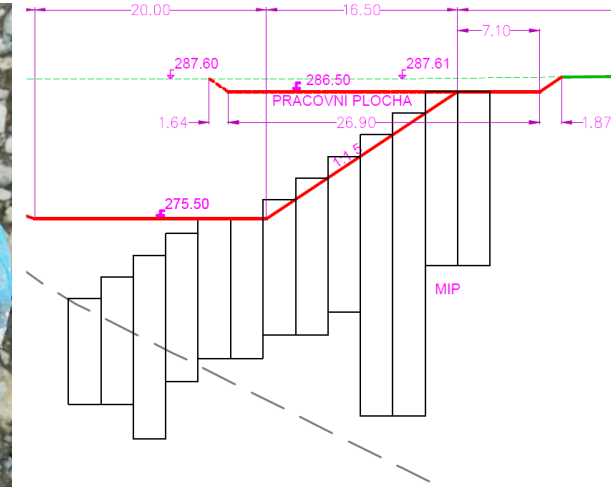
- **Dürer Park, Budapest, Hungary**
- Deep excavation: slurry walls 40 cm thickness, jet grouting, anchors
- Construction period: 05/2021 – 10/2021



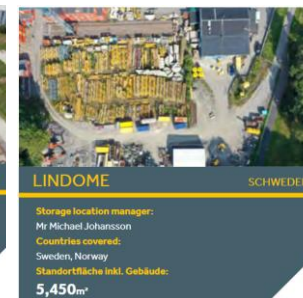
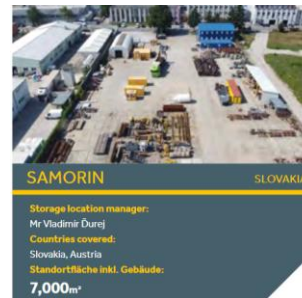
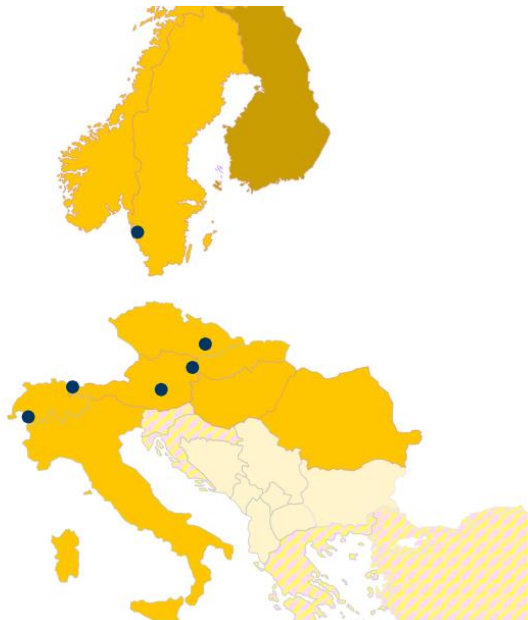
- **EUROVEA II, Bratislava, Slovakia**
- Deep excavation: single pile wall with jet grouting columns up to 30 m
- Foundation: totally > 21.000 m cased piles up to 41 m drilling depths with polymer slurry and CFA piles with diameter 88 cm up to 24 m depth
- Dewatering with 14 pumping wells for 858 days
- Construction period: 03/2019 – 02/2021



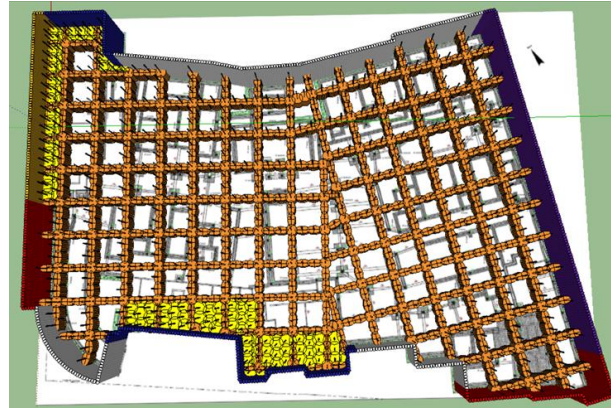
- **SO 02 Trial area, Coal Mine Bilina, Czech Republic**
- Landfill stabilization
- Mixed-in-Place (MIP) panels as cement stabilization of landfill area
- 5.665 m² MIP elements up to 23.5 m depth
- Construction period: 07-08/2020



- **Keller South-East Europe & Scandinavia – headquarters in Vienna**
- Support of nearly 900 construction sites each year

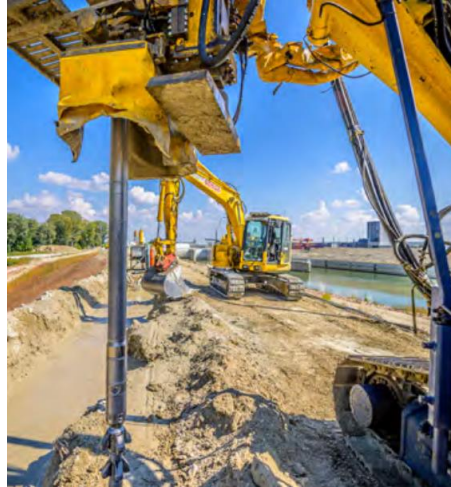


■ St Barthélemy Island Project – Keller South-West Europe



- Foundation of new hotel complex with jet grouting
- Support of Keller with Austrian ACI® specialist

■ Moson Lock, Hungary



- A lock in a tributary of the Danube river as part of an environmental rehabilitation project
- Jet grouting sealing slab – support of Keller with personnel and equipment

■ SMS2a, Norway



- Part of the intercity development project, which is part of the largest transport project in Norway, consisting of 270 km of new double-track rail
- Support of Keller with personnel and equipment

■ Eurovea 2, Slovakia



- Construction pit for a car park with four underground floors – part of the Eurovea 2 (public square, residential and commercial buildings)
- Support of Keller with anchorage know-how

■ Le Grand Paris (LGP) – Keller France



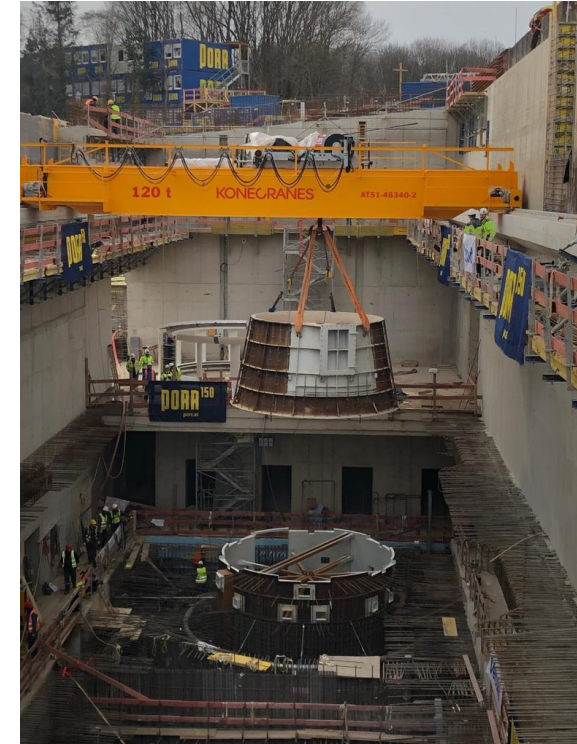
- Extension of the existing metro line in Paris
- Cooperation started in the tendering phase and ended with the deployment of site personnel and equipment on site

■ HPP Töging am Inn, Germany

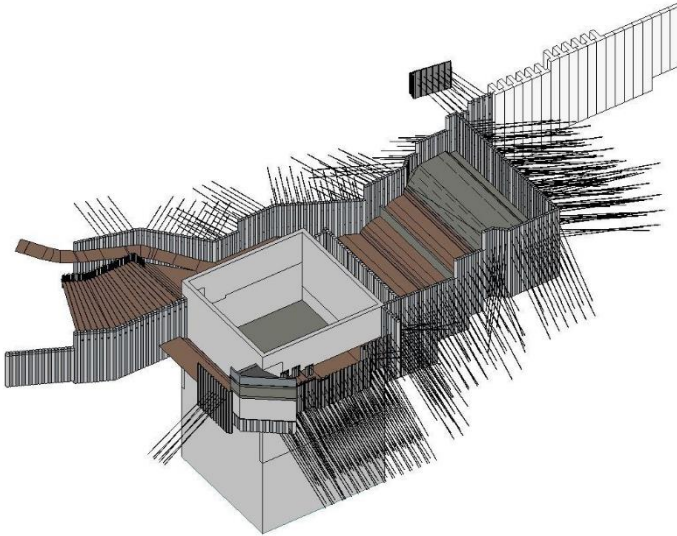
The nearly 100 years old hydro power plant at river Inn in Töging, Bavaria, was reconstructed in the years 2020 to 2022.

For the construction of the new power house heavy foundation works were necessary to depths of more than 70 meters. The complex ground and groundwater conditions on site were most challenging.

Diaphragm walls with 1.0 m thickness, jet grouting, anchors, board piles and complex dewatering processes were performed by up to 100 employees.



- **HPP Töging am Inn, Germany**



■ Motorway D4R7, Slovakia

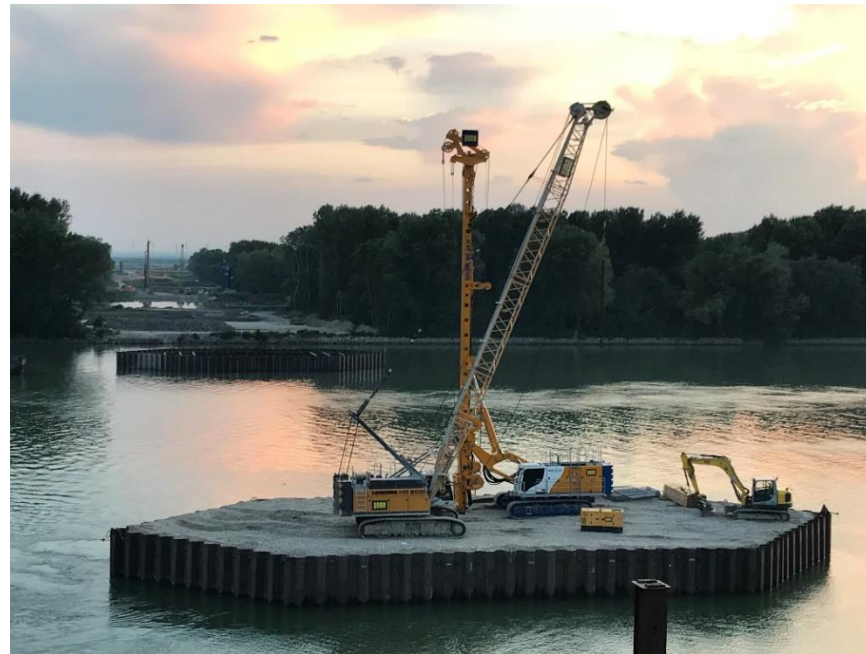
The construction of the motorways D4 and R7 in the area of Bratislava required more than 30 deep excavations for bridge piers.

Four out of them serve for the foundation of the piers in the Danube river for the new bridge over the Danube.

Numerous sheet pile walls, jet grouting works and bored piles with a diameter of up to 180 cm were executed in the years 2017-2019.



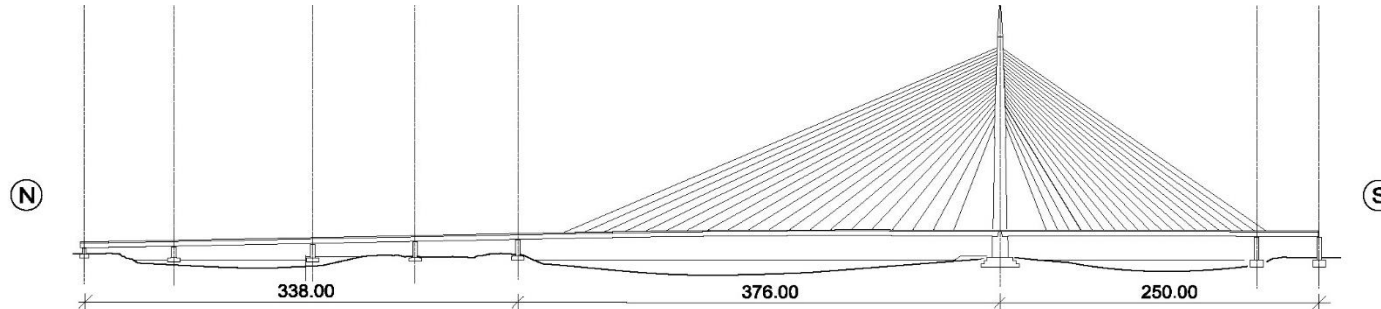
- **Motorway D4R7, Slovakia**



■ Sava Bridge, Serbia

The construction works for the foundation of the new bridge over the river Sava in Belgrade were executed in 2008 and 2009. This bridge is still one of the largest cable stayed bridges in Europe.

The scope of work comprised the construction of the foundation for the 200 m tall pylon and six other piers of the bridge. Therefore diaphragm walls, piles, jet grouting and sheet pile foundations were carried out.



- **Sava Bridge, Serbia**



■ FAIR PARTICLE ACCELERATOR FACILITY

Darmstadt, Germany



DATA AND FACTS

- **Construction period:** 05/2017 – 12/2022
- **Client:** FAIR GmbH, Darmstadt
- **Work performed:**
 - More than 300 drilled wells
 - Complex dewatering system

■ KRIEGSSTRASSE ROAD TUNNEL (COMBINED SOLUTION FOR KARLSRUHE)

Karlsruhe, Germany



DATA AND FACTS

- **Construction period:** 07/2017 – 09/2021
- **Client:** KASIG (Karlsruher Schieneninfrastruktur-Gesellschaft bmH), Karlsruhe
- **Work performed:**
 - Silica gel grouting for 35,000 m² horizontal sealing slab (ISI - Insond Seal Inject soft gel injection)
 - Jet grouting

■ TUNNEL BURG STABILIZATION

Küssnacht, Switzerland



DATA AND FACTS

- **Construction period:** 02/2018 – 05/2019
- **Client:** Joint Venture Baresel & Heitkamp
- **Work performed:**
 - Horizontal jet grouting
 - Preventer-protected injection boreholes
 - Preventer-protected drainage boreholes

■ GLORIA BERLIN JET GROUTING

Berlin, Germany



DATA AND FACTS

- **Construction period:** 02/2018 – 04/2019
- **Client:** Centrum Ku'Damm 12, 13-15 GmbH und Co. KG
- **Work performed:**
 - Jet grouting for underpinning
 - Horizontal jet grouting slab

■ A63 CASTLE STREET IMPROVEMENT

Kingston upon Hull, United Kingdom



DATA AND FACTS

- **Construction period:** 2020 - 2023
- **Client:** Balfour Beatty / National Highways
- **Work performed:**
 - Soil stabilization (Dry Deep Mixing)
 - D-Wall
 - Tension piles
 - Horizontal jet grouting slab

■ STUREGALLERIAN FOUNDATION WORKS

Stockholm, Sweden



DATA AND FACTS

- **Construction period:** 2021 - 2022
- **Client:** Sturegallerian Aktiebolag
- **Work performed:**
 - Jet grouting for underpinning

■ Composition & Target Group

- Young professionals dedicated to all branches of geotechnical engineering
- Universities & additional members from public & private sector

■ Mission & Aim

- Connect the next generation of geotechnical engineers
- Establish inter-generational communication channels
- Co-operational sharing of knowledge & ideas

■ Activities & Events

- Symposium, field trips & expert lectures
- Next steps: Fireside chats & annual award



Hybrid Young Members Symposium
(Austrian Geotechnical Society, 2021)

Important Conferences

■ Past

- 1st Danube European Conference, Vienna 1964
- 2nd Danube European Conference, Vienna 1968
- 6th European Conference on Soil Mechanics and Foundation Engineering, Vienna 1976
- 16th European Young Geotechnical Engineers Conference, Vienna 2004
- 15th Danube European Conference, Vienna 2014
- 26th European Young Geotechnical Engineers Conference, Graz 2018
- 40 Years of Roller Integrated Continuous Compaction Control (CCC), Vienna 2018

■ Present

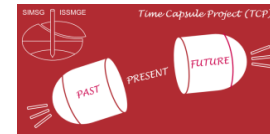
- Bi-annual Austrian Conference on Geotechnical Engineering in Vienna since 1997 including the **Vienna Terzaghi Lecture**
- Annual Christian Veder Colloquy, Graz since 1985



Austrian
Geotechnical
Society

OIAV
AUSTRIAN ASSOCIATION OF
ENGINEERS AND ARCHITECTS

Time Capsule Project (TCP)



77

BID for 21st ICSMGE 2026

INVITATION

EXECUTIVE SUMMARY

Dear Members of ISSMGE,

In 1925 Karl Terzaghi published the book „Erdbaumechanik auf bodenphysikalischer Grundlage“. On the occasion of the 100th Anniversary of this publication the Austrian Geotechnical Society as a member of the Austrian Association of Engineers and Architects and the Austrian Society for Geomechanics would like to take this opportunity to host the 21st International Conference on Soil Mechanics and Geotechnical Engineering (ICSMGE) in Vienna, Austria, due to the COVID-19 situation shifted to 2026.

The suggested theme of the conference **Geotechnical Challenges in a Changing Environment** provides a platform for developing new strategies for geotechnical engineering to cope with increasingly complex environmental requirements, last but not least in view of the consequences of the corona pandemic. Vienna has an excellent reputation for being a top conference destination for holding conferences with several thousand participants and has been ranked as one of the worldwide top venues for more than 15 years. In addition, Vienna is a world class tourist attraction with a long history in music, museums and architecture.

- An experienced Organizing Committee under the leadership of Helmut F. Schweiger has been set up to ensure a smooth organisation of the conference.
- The Scientific Committee under the leadership of Dietmar Adam will guarantee a high standard of conference papers and make provisions that a large number of papers can be presented at the conference.
- A Young Geotechnical Engineers conference will be held prior to the main conference under the leadership of Franz Tschuchnigg who is dedicated to organize a memorable event for the younger generation of geotechnical engineers.
- Support of the local government will allow for moderate conference fees and support for developing countries.

We kindly ask for your support for this 100th anniversary initiative and look very much forward to welcoming you to the 21st ICSMGE in Vienna, Austria in 2026.



Heinz Brandl

Heinz Brandl
Honorary President Austrian
Geotechnical Society



Helmut F. Schweiger

Helmut F. Schweiger
President Austrian
Geotechnical Society



Dietmar Adam

Dietmar Adam
General Secretary Austrian
Geotechnical Society



Wulf Schubert

Wulf Schubert
President Austrian Society
for Geomechanics

1925
Erdbaumechanik
auf bodenphysikalischer Grundlage

K. Terzaghi
Dr. Ing. Karl Terzaghi
Professor and Professor in Geotechnical Engineering
at the University of Vienna

1925 - 2025
100th ANNIVERSARY OF TERZAGHI'S
"ERDBAUMECHANIK"

XXI ICSMGE
VIENNA
AUSTRIA

GEOTECHNICAL CHALLENGES
IN A CHANGING ENVIRONMENT



INVITATION TO VIENNA

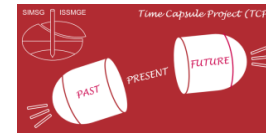




Austrian
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AUSTRIAN ASSOCIATION OF
ENGINEERS AND ARCHITECTS

Time Capsule Project (TCP)



78

Austrian Geotechnical Society (1936 - 2022)

Presidents

K.v. Terzaghi 1936-1938

re-established in 1950

W. Aichhorn 1950-1972

H. Brandl 1972-2015

H.F. Schweiger since 2015

helmut.schweiger@tugraz.at

Secretaries

W. Steinbrenner 1950-1972

M. Fross 1972-2004

D. Adam since 2004

dietmar.adam@tuwien.ac.at

www.oiaiv.at/fachgruppen/fg-geotechnik/

Postal Address:

Austrian Geotechnical Society
ÖIAV - Österreichischer Ingenieur-und Architekten-Verein
(Austrian Association of Engineers and Architects)
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A-1010 Vienna